

# Euler-Euler and Euler-Lagrange Modeling of Wood Gasification in Fluidized Beds

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CFB-9, May 13-16, 2008, Hamburg

# Overview

- Motivation
- Modeling approaches
  - Euler-Lagrange / Discrete Element Method (DEM)
  - Euler-Euler
- Results
- Summary and outlook

# Motivation - simulation of wood gasification

- Renewed interest in producing gas from biomass
- Gasification in fluidized bed reactors
- Lack of detailed knowledge about the complex interactions between heterogeneous reactions and the fluid mechanics in fluidized beds
- Develop closure laws for large scale models

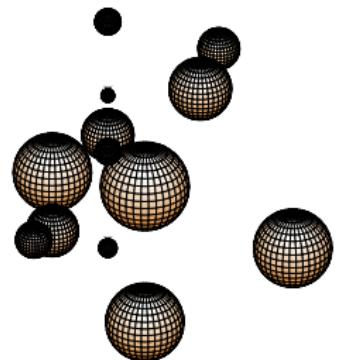
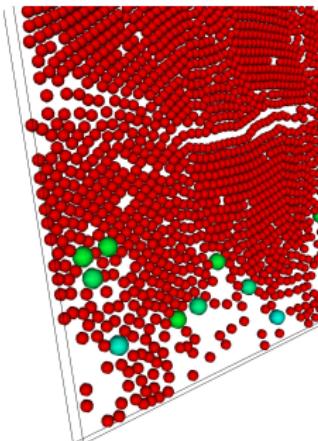
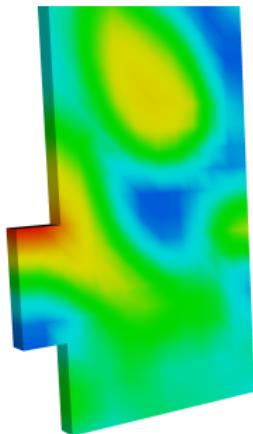
# CFD modeling for particulate flow

Continuum models

Euler-Lagrange

DNS

tractable problem size



computational cost

# Euler-Lagrange model

Basis:

OpenFOAM ([www.openCFD.co.uk/openfoam](http://www.openCFD.co.uk/openfoam))

Modules:

- ① Solver for the gasphase (OpenFoam)
- ② Lagrangian particle tracking / DEM (OpenFOAM)
- ③ Particle combustion / gasification model

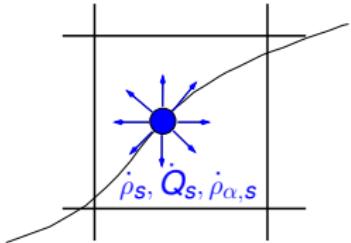
(here: simple zero dimensional particle model)

# Euler-Lagrange model – gasphase

Mass / momentum balance:

$$(\rho\epsilon)_t + \nabla \cdot \epsilon\rho u = \epsilon\dot{\rho}_s$$

$$(\epsilon\rho u)_t + \nabla \cdot \{\epsilon\rho uu\} + \nabla p - \nabla \cdot \tau + \epsilon\rho g = F_s$$



Energy / species balance:

$$(\rho\epsilon E)_t + \nabla \cdot [(\rho E + p)\epsilon u] + \nabla \cdot q = \dot{Q}_s$$

$$(\rho\epsilon u Y_\alpha)_t + \nabla \cdot [\rho\epsilon Y_\alpha u] - \epsilon\dot{w}_\alpha = \epsilon\dot{\rho}_{\alpha,s}$$

# Euler-Lagrange model – particle tracking

- Equation of motion for every single particle

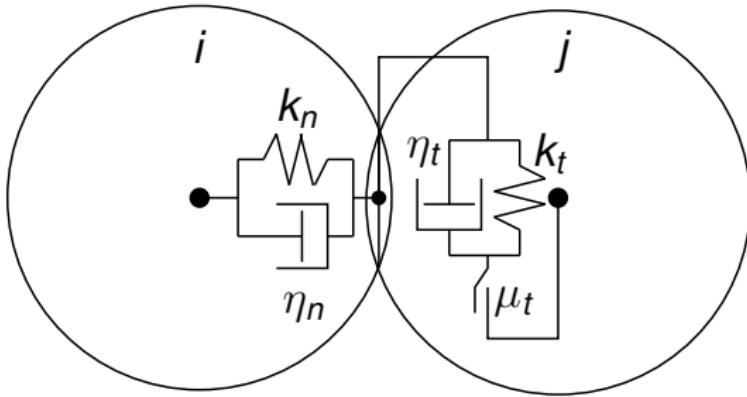
$$m_i \frac{d\vec{v}_i}{dt} + \vec{v}_i \frac{dm_i}{dt} = \sum_j \vec{F}_{ij}$$

$$J_i \frac{d\vec{\omega}}{dt} + \vec{\omega} \frac{dJ_i}{dt} = \sum_j \vec{M}_{ij}$$

- Fluid dynamic forces ( drag, buoyant, Magnus, etc.) with empirical correlations
- Contact forces via spring-damper modell
- Multiple particle contacts possible

# Euler-Lagrange – contact forces by DEM

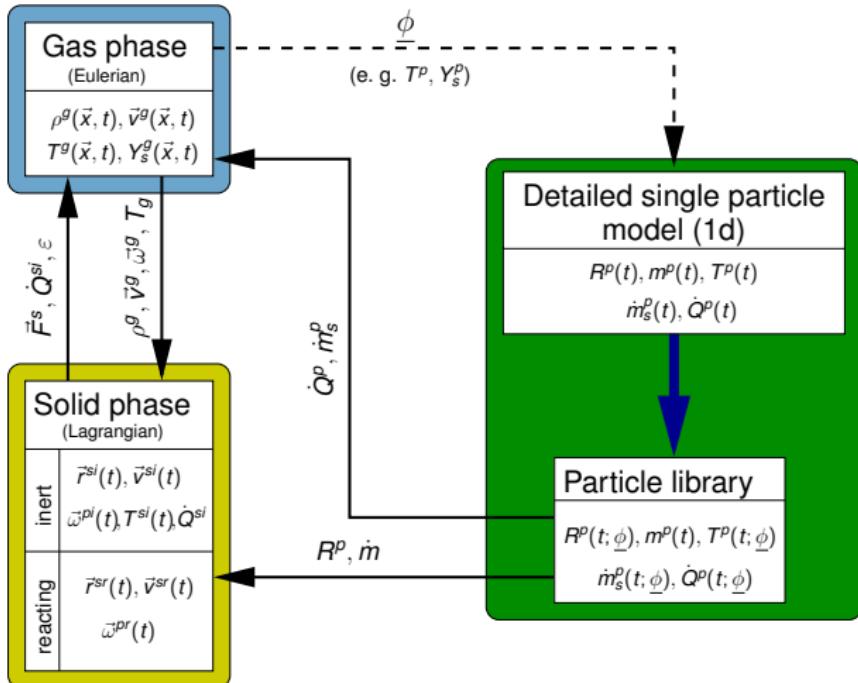
(Cundall & Strack, 1979)



$$\vec{F}_{ij}^n = k_n \delta \vec{n} + \eta_n \vec{v}_{ij}^n$$

$$\vec{F}_{ij}^t = \min \left( \mu_t |\vec{F}_{ij}^n| \vec{t}, \eta_t |\vec{v}_{ij}^t| \right)$$

# Euler-Lagrange model – coupling



## Euler-Euler model

- Public Domain Code MFIX ([www.mfix.org](http://www.mfix.org))
- 1 gas phase
- 3 solid phases: wood (4mm), 2 x charcoal (1mm, 2mm)
- 5 homogeneous gas phase reactions (rev.),  
4 heterogeneous reactions carbon
- Models for primary and secondary pyrolysis

# Gas phase chemistry

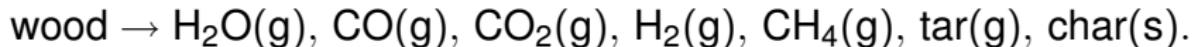
Simple reaction mechanism

Species: H<sub>2</sub>, O<sub>2</sub>, N<sub>2</sub>, CO, CO<sub>2</sub>, CH<sub>4</sub>, H<sub>2</sub>O, tar

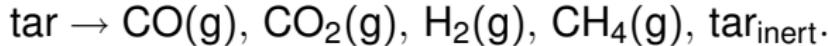
1. 2 CO + O<sub>2</sub> ⇌ 2 CO<sub>2</sub>
2. 2 H<sub>2</sub> + O<sub>2</sub> ⇌ 2 H<sub>2</sub>O
3. 2 CH<sub>4</sub> + 3 O<sub>2</sub> ⇌ 2 CO + 4 H<sub>2</sub>O
4. CO + H<sub>2</sub>O ⇌ H<sub>2</sub> + CO<sub>2</sub>
5. CH<sub>4</sub> + H<sub>2</sub>O ⇌ CO + 3 H<sub>2</sub>

# Pyrolysis / heterogeneous reactions

Primary pyrolysis (Grönli, Melan (2000))



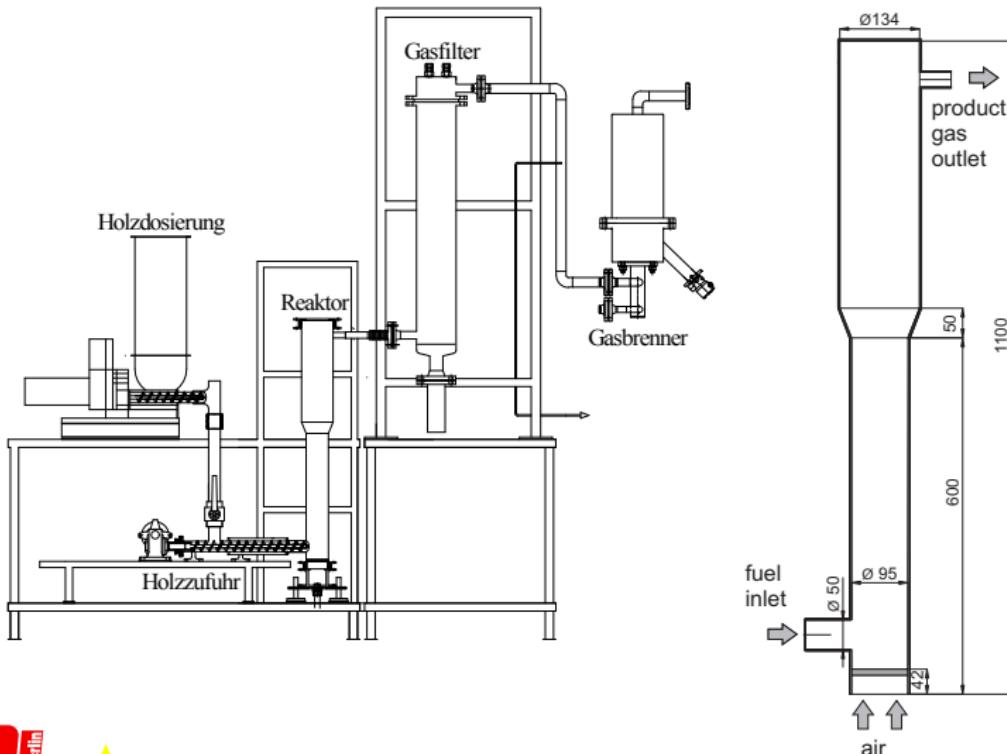
Secondary pyrolysis (Boroson et al. (1989))



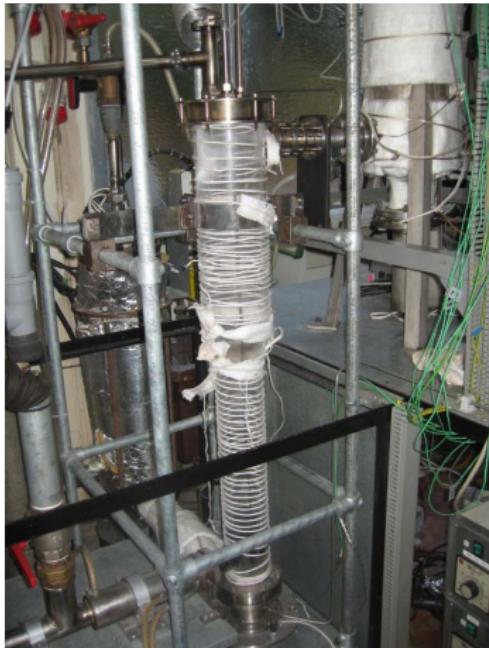
Heterogeneous reactions



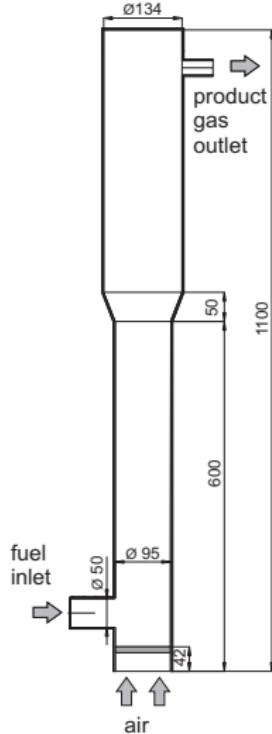
# Reactor at the department



## Reactor at the department



# Reactor – inlet boundaries



wood inflow:

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wood  $T = 150 \text{ }^{\circ}\text{C}$ ,  $v = 0.08 \text{ cm/s}$

bulk density  $0.385 \text{ g/cm}^3$

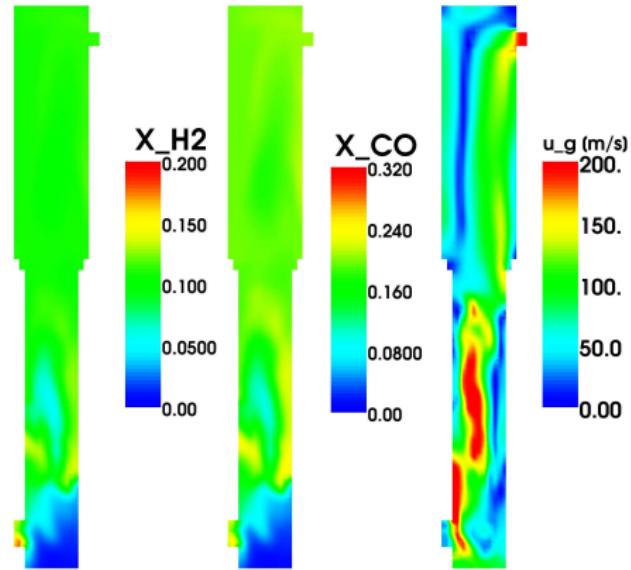
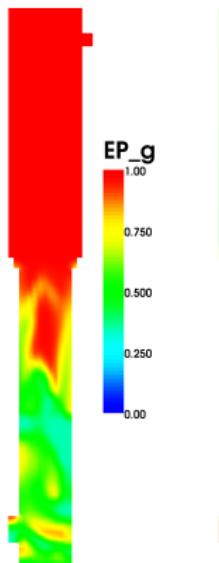
air inflow:

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gas species 21%  $\text{O}_2$ , 79%  $\text{N}_2$

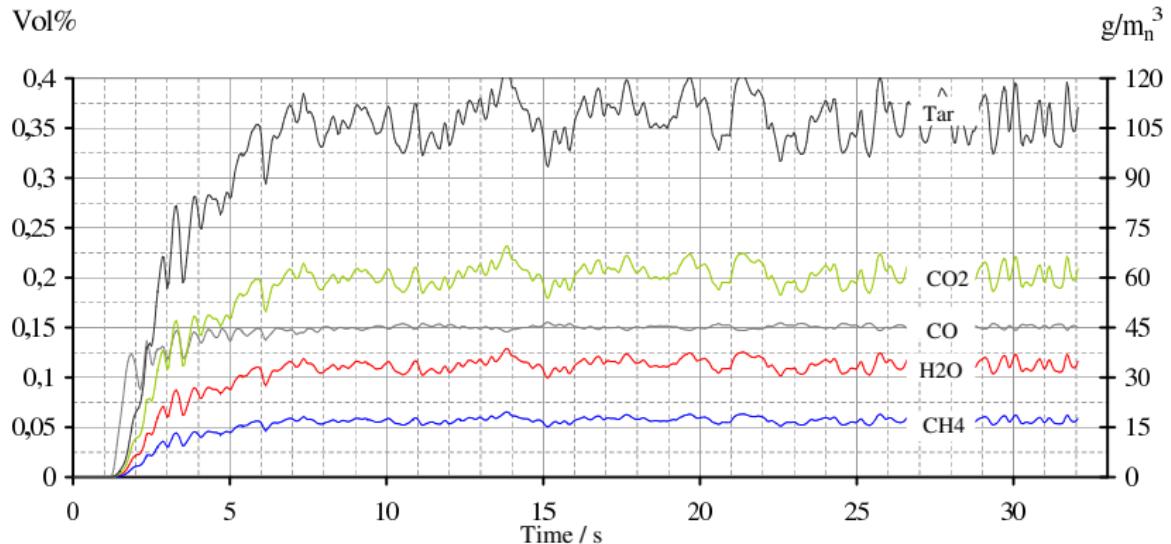
$T = 400 \text{ }^{\circ}\text{C}$ ,  $v = 25 \text{ cm/s}$

## Results - Euler-Euler model

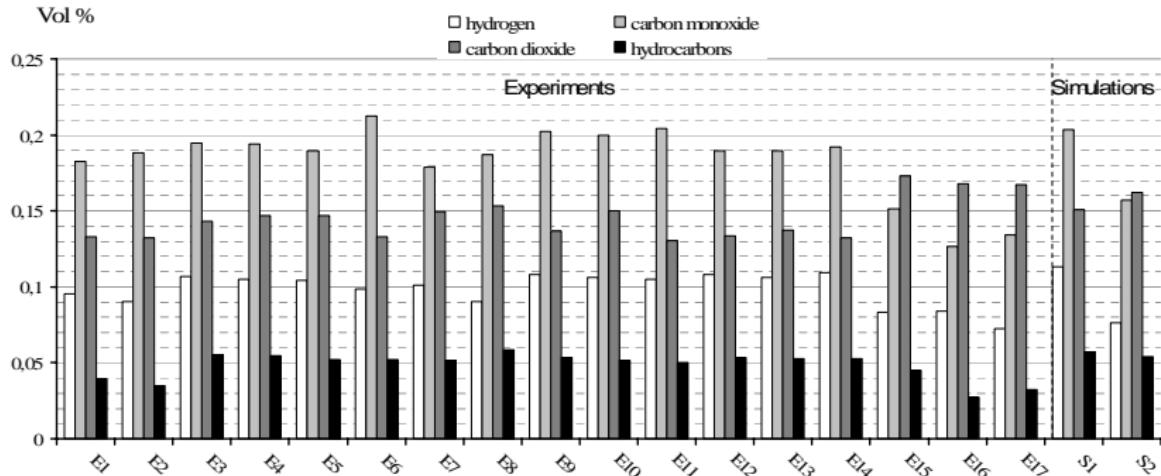


▶ play

# Results – exhaust gas composition



# Results - Euler-Euler model

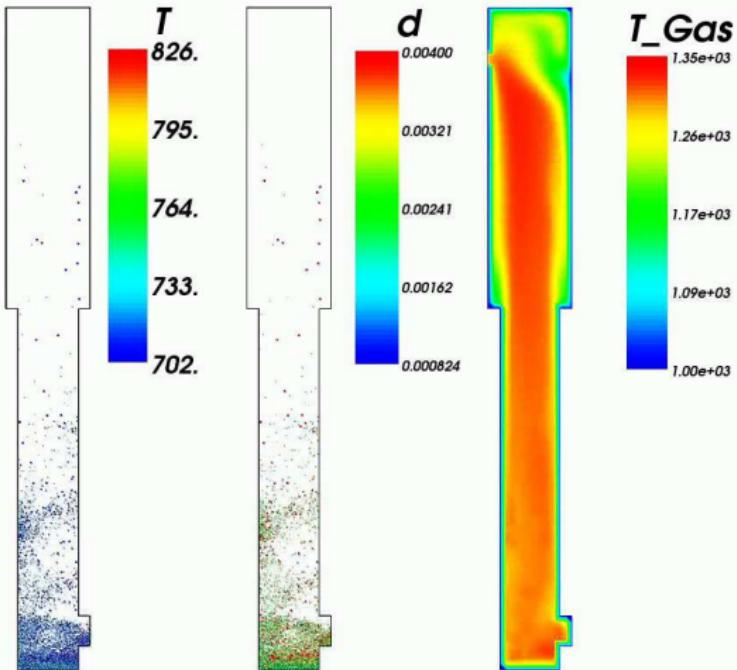


# Euler-Lagrange / DEM – results

Model assumptions:

- proportional particle massloss and shrinking
- transient calculation of particle mass-loss and energy
- no heterogeneous reaction (in progress)
- no particle-particle heat transfer
- no radiation

## Euler-Lagrange / DEM – results



## Summary and outlook

- Euler-Lagrange and Euler-Euler model for wood gasification in fluidized beds
- Euler-Euler: reasonable agreement with experimental data
- Euler-Lagrange: allows detailed investigation of particle/chemistry/gas phase interactions
- Refined chemistry
- Parallelization of the DEM modell
- Quantitative comparison between Euler-Euler, Euler-Lagrange/DEM und experiments
- Coupling Euler-Lagrange with Euler-Euler methods

The financial support of the  
Deutsche Bundesstiftung Umwelt (DBU)  
is gratefully acknowledged!

# Governing equations – Euler-Euler model

Species mass balance gas phase

$$\frac{\partial}{\partial t}(\epsilon_g \rho_g Y_{gs}) + \nabla \cdot (\epsilon_g \rho_g \vec{v}_g Y_{gs}) = \nabla \cdot (D_{gs} \nabla Y_{gs}) + R_{gs}$$

Mass balance solid phase

$$\frac{\partial}{\partial t}(\epsilon_m \rho_m Y_{ms}) + \nabla \cdot (\epsilon_m \rho_m \vec{v}_{sm} Y_{ms}) = \nabla \cdot (D_{ms} \nabla Y_{ms}) + R_{ms}$$

# Governing equations – Euler-Euler model

Momentum balance solid phase

$$\frac{\partial}{\partial t}(\epsilon_m \rho_m \vec{v}_m) + \nabla \cdot (\epsilon_m \rho_m \vec{v}_m \vec{v}_m) = -\epsilon_m \nabla p_m + \nabla \cdot \bar{\tau}_m - \sum_{\substack{l=1 \\ l \neq m}}^{n_m} \vec{I}_{ml} + \vec{I}_{gm} + \epsilon_m \rho_m \vec{g}$$

# Governing equations – Euler-Euler model

Energy balance gas phase

$$\epsilon_g \rho_g c_{pg} \left( \frac{\partial T_g}{\partial t} + \vec{v}_g \cdot \nabla T_g \right) = -\nabla \cdot \vec{q}_g + \sum_{m=1}^{N_m} \gamma_{gm} (T_m - T_g) - \Delta H_g$$

Energy balance solid phases

$$\epsilon_m \rho_m c_{pm} \left( \frac{\partial T_m}{\partial t} + \vec{v}_m \cdot \nabla T_m \right) = -\nabla \cdot \vec{q}_m - \gamma_{gm} (T_m - T_g) - \Delta H_m$$