

A comprehensive model for large-scale CFB units

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Aim & Background

→ Comprehensive

→ Universal

Phenomenology

→ Steady-state, 3-dimensional



HEAT BALANCE

→ Operation-orientated set of inputs

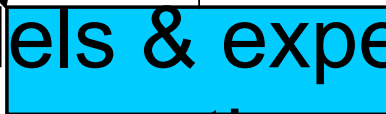
→ Low calculation time (~min)

Gas generation

Flows & Concentrations

T

- Submodels & experimental data from literature
- Human expertise at Chalmers



Geometry



CFB comprehensive modeling

-1996



Hannes (Preto)

1.5-D Riser

1989-present



Werdermann, Knöbig,
Lücke, Wischnewski
(Werther, Hartge)

3-D Loop

1998-2001



Joule III participants

1.5-D Riser

2005-present



Pallarès
(Johnsson)

3-D Loop

Chalmers model development



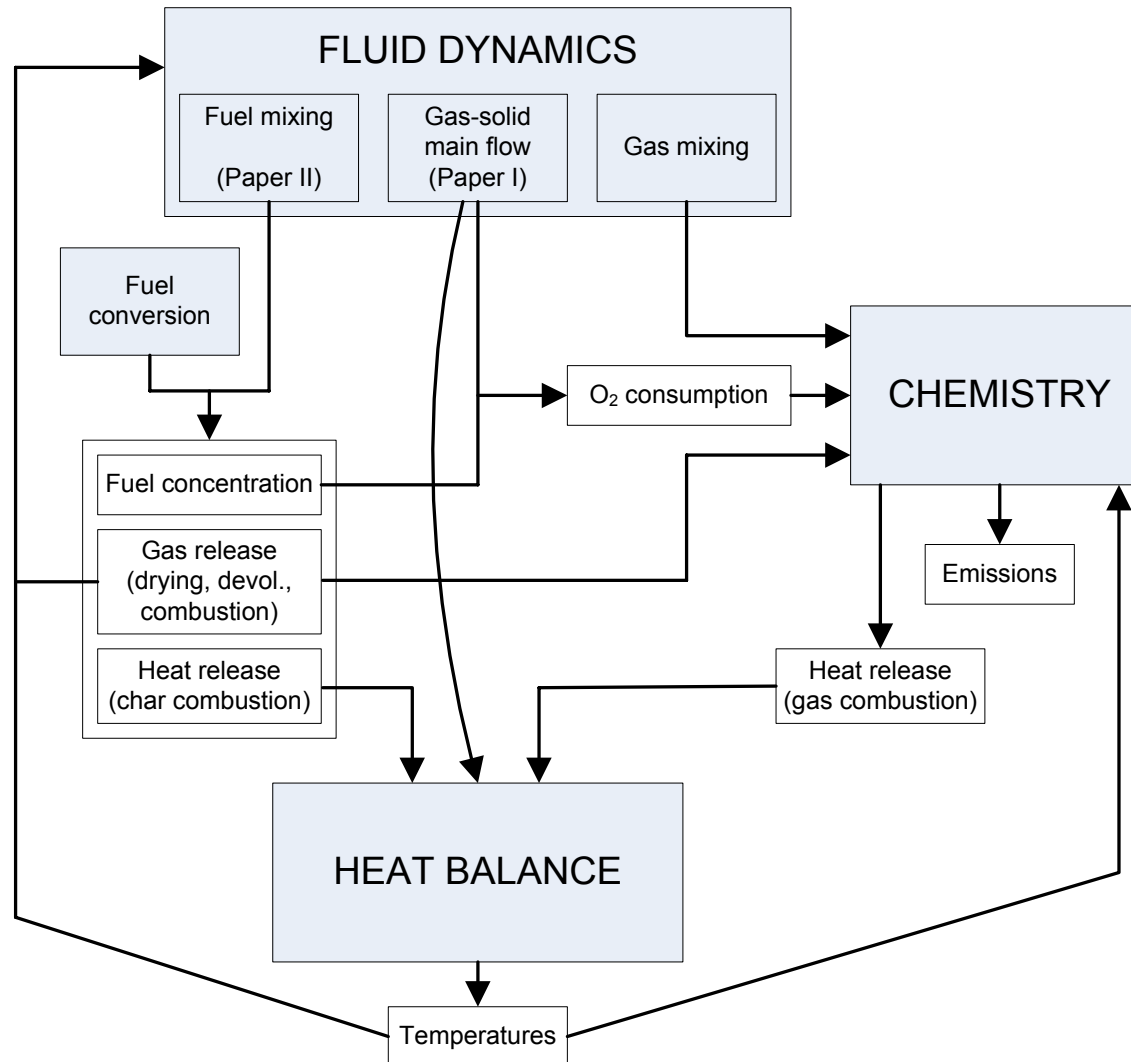
1998-2001: Submodel for
CFB fluid dynamics



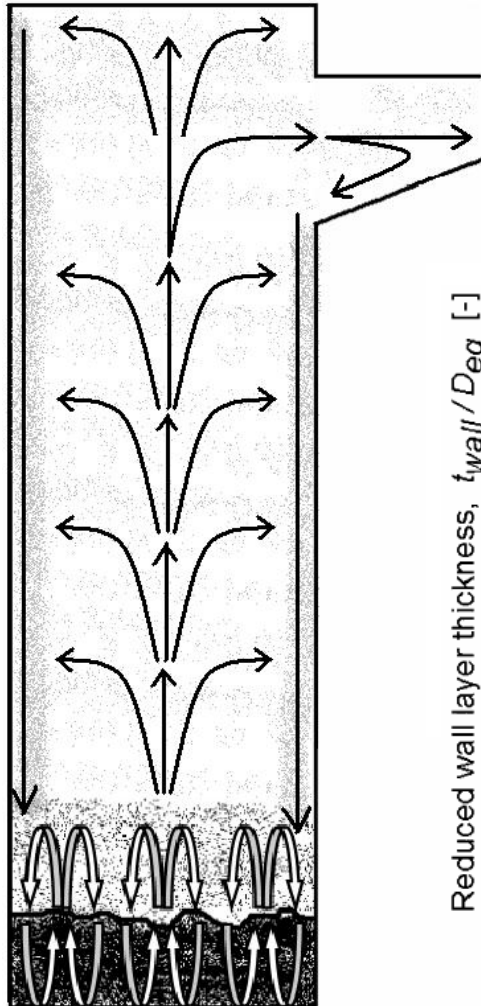
2005-2007: P1. Overall CFB model (PhD)

2008-2009: P2. Refined CFB model

Submodels coupling



Inert solids fluidynamics



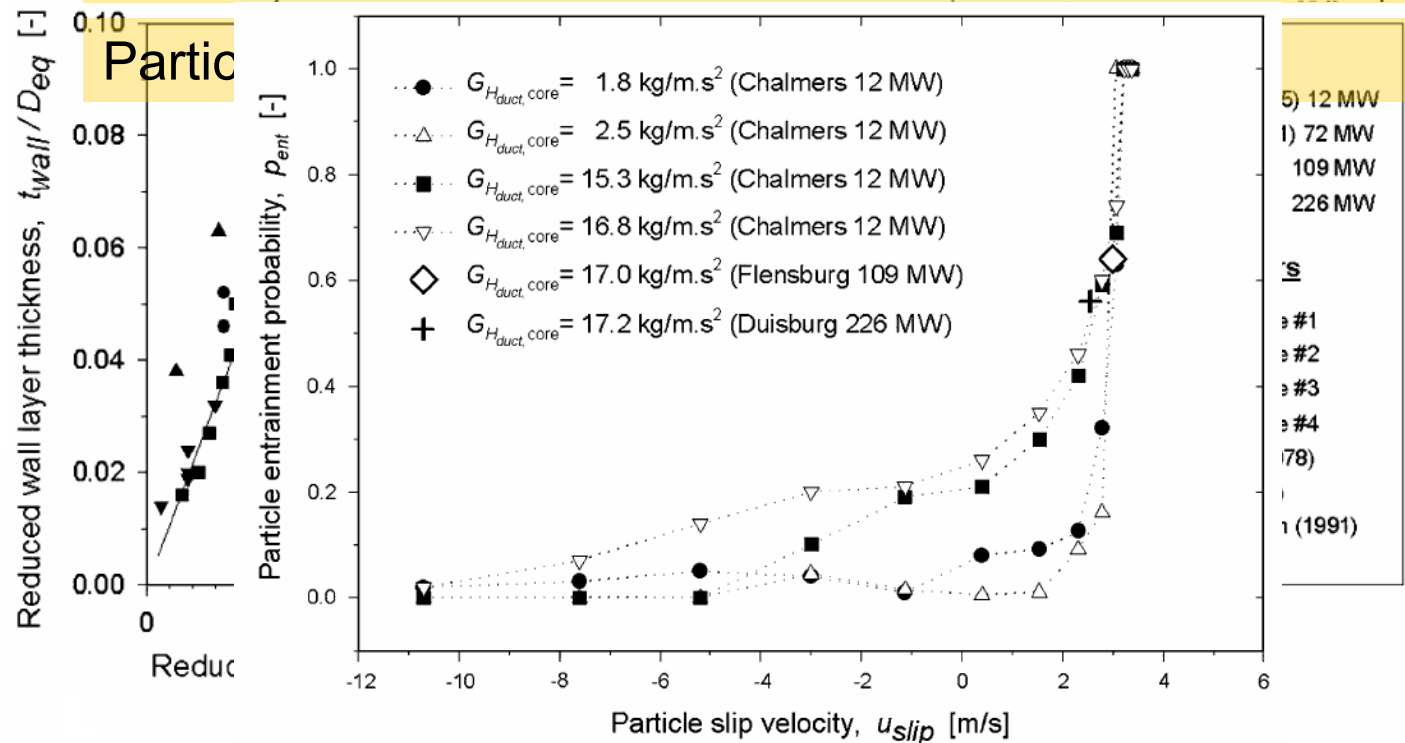
Cluster & disperse phases (Johnsson and Leckner)

Wall layer thickness – Correlation

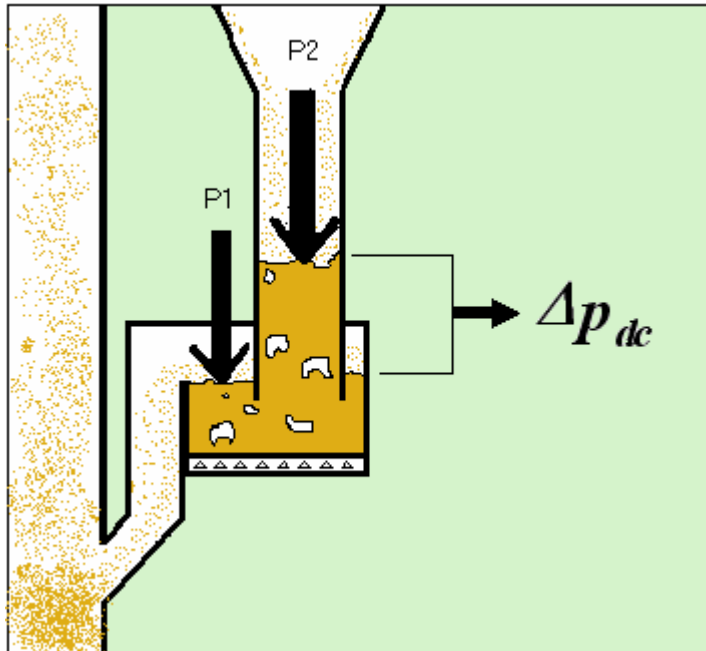
Backflow effect - Correlation

Chalmers 12 MW_{th} CFBC

$u_0 = 2.7 \text{ m/s}$, $d_s = 320 \text{ }\mu\text{m}$



Inert solids fluid dynamics



Pressure balance on circulating loop

$$\downarrow$$
$$\Delta p_{dc}$$
$$\downarrow$$
$$m_{dc}$$
$$\downarrow$$

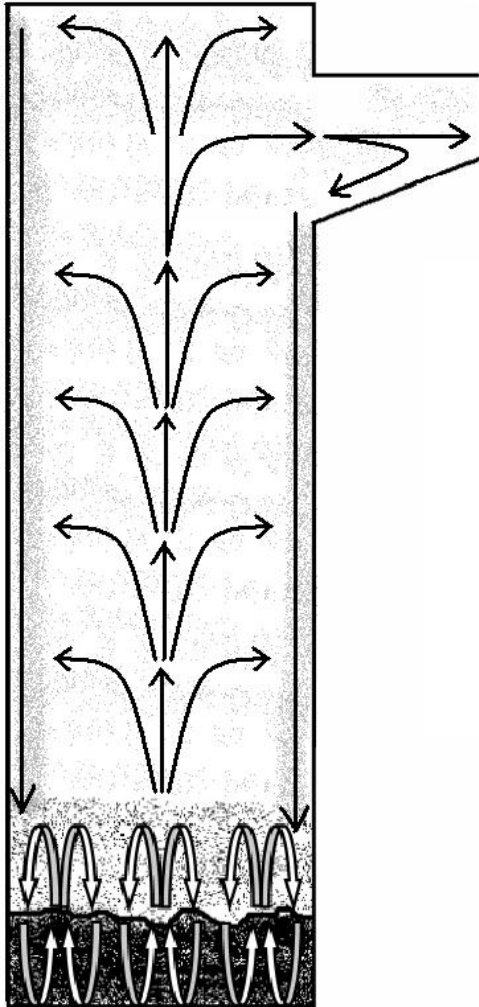
Population balance on circulating loop

Pallarès, D., Johnsson, F.

“Macroscopic modeling of fluid dynamics in large-scale circulating fluidized beds”

Progress in Energy and Combustion Science 32 (2006)

Fuel mixing & conversion



- Varying particle size & density

Dynamical simulation of the mixing of a fuel batch during all its burnout time is required.

Continuous fuel feeding is later approximated by superposition of time-delayed fuel batches.

- Strong horizontal gradients

Horizontal fuel dispersion is approximated macroscopically by Brownian diffusion process ($D_h \sim 0.1 \text{ m}^2/\text{s}$).

Fuel mixing & conversion

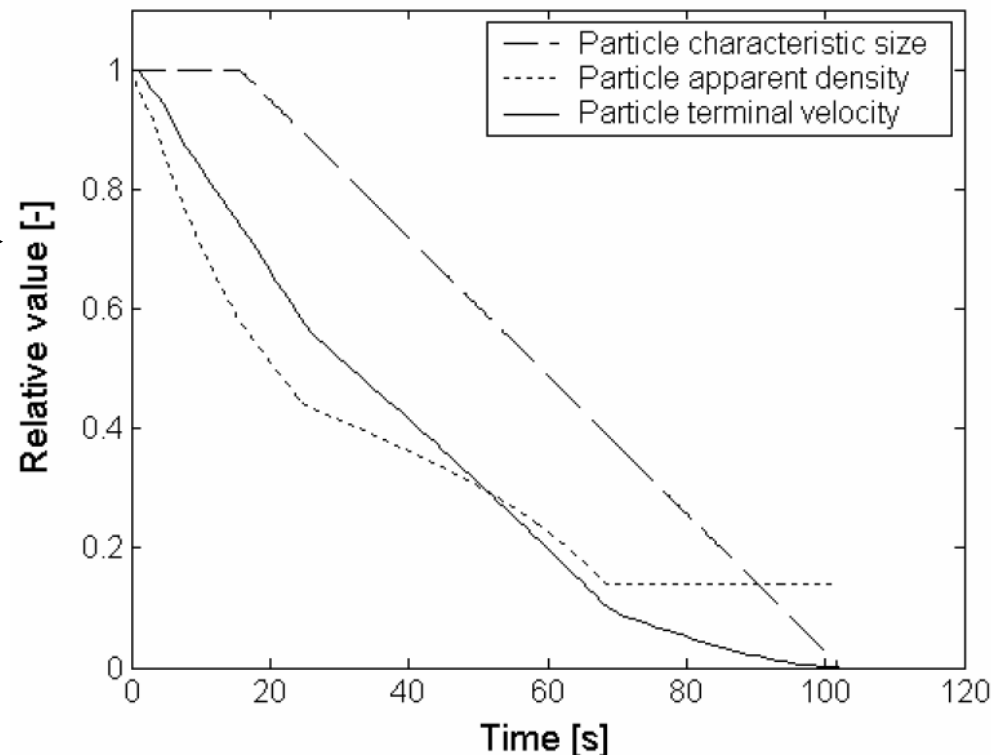
Palchonok *et al.*

- Fuel particle approximated as ∞ -plane, ∞ -cylinder or sphere
- Quasi-steady state

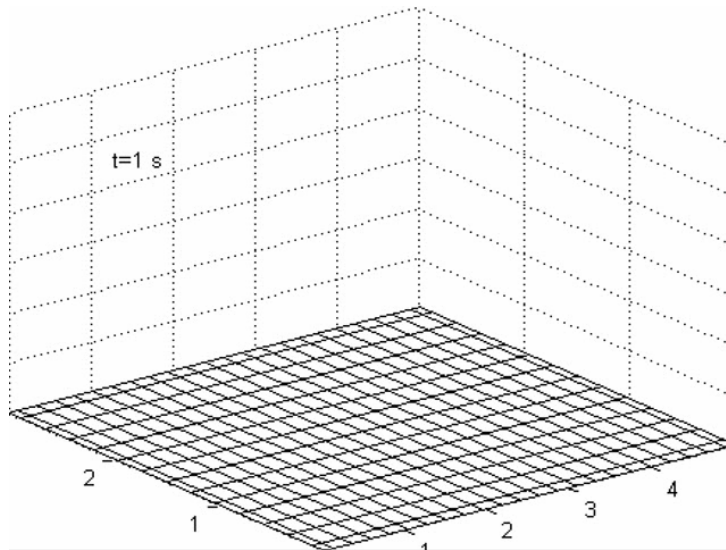


$$\frac{1}{r^n} \frac{\partial}{\partial r} \left(r^n k_c \frac{\partial T}{\partial r} \right) - \frac{1}{r^n} \frac{\partial}{\partial r} \left(r^n u_g \rho_g c_{pg} T \right) = 0 \longrightarrow$$

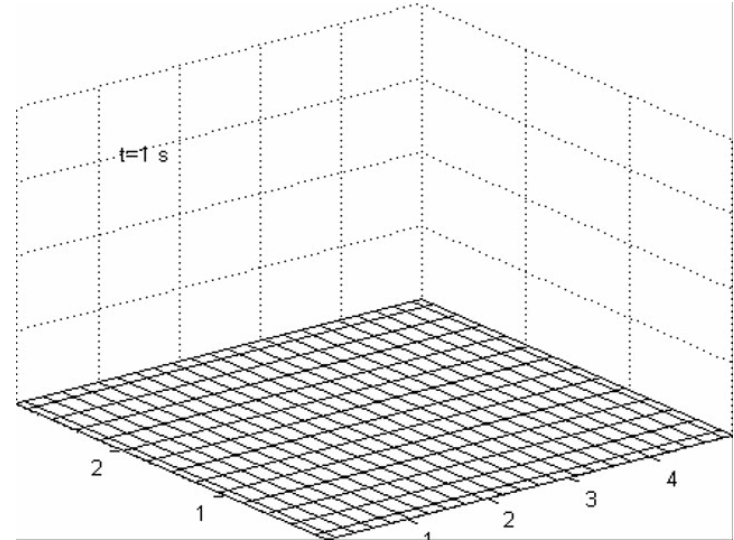
(analytical solution)



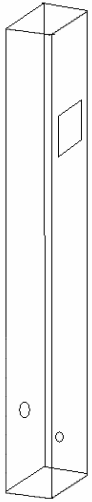
Fuel mixing & conversion



Fuel batch



Superposition of
time-delayed fuel batches



Fuel mixing & conversion

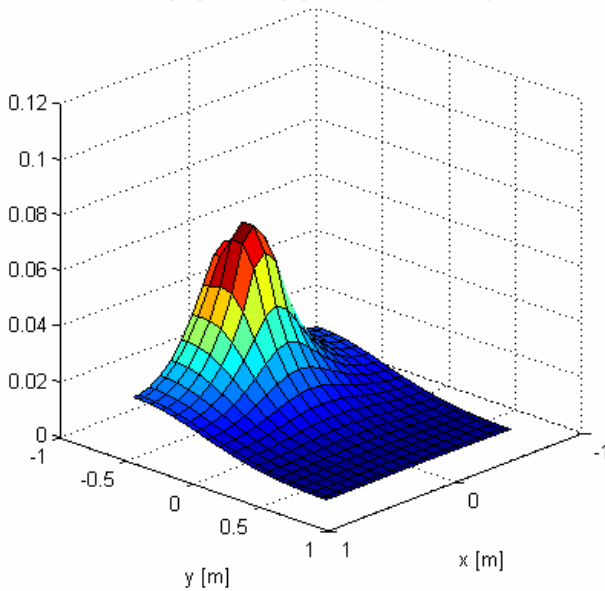
Distribution of gas releases in bottom bed

Moisture

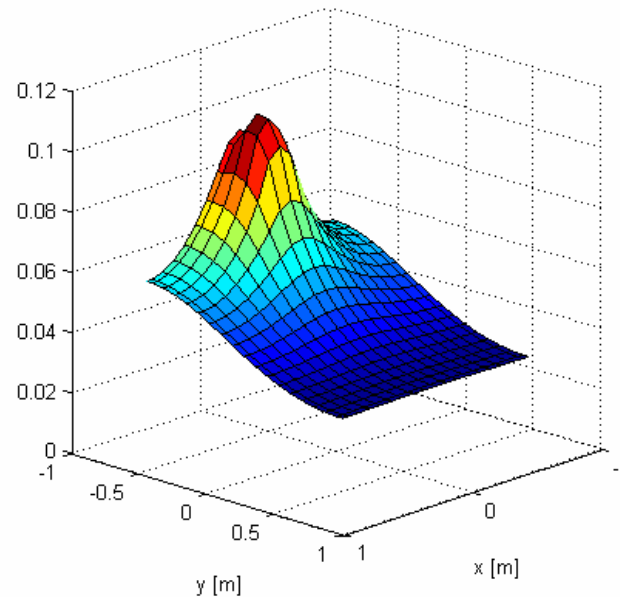
Volatiles

CO₂

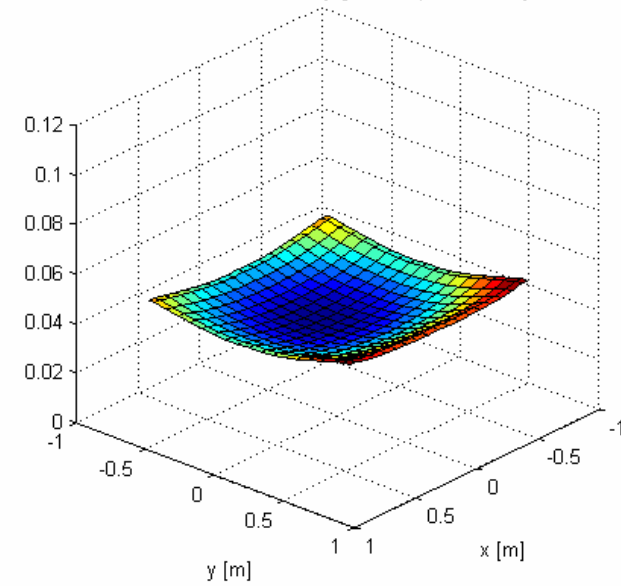
Drying release [kg field in particle/m³s]



Devolatilization release [kg field in particle/m³s]

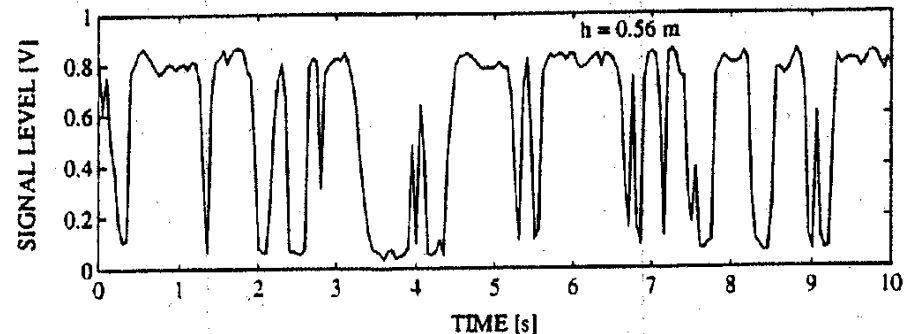


Combustion release [kg field in particle/m³s]

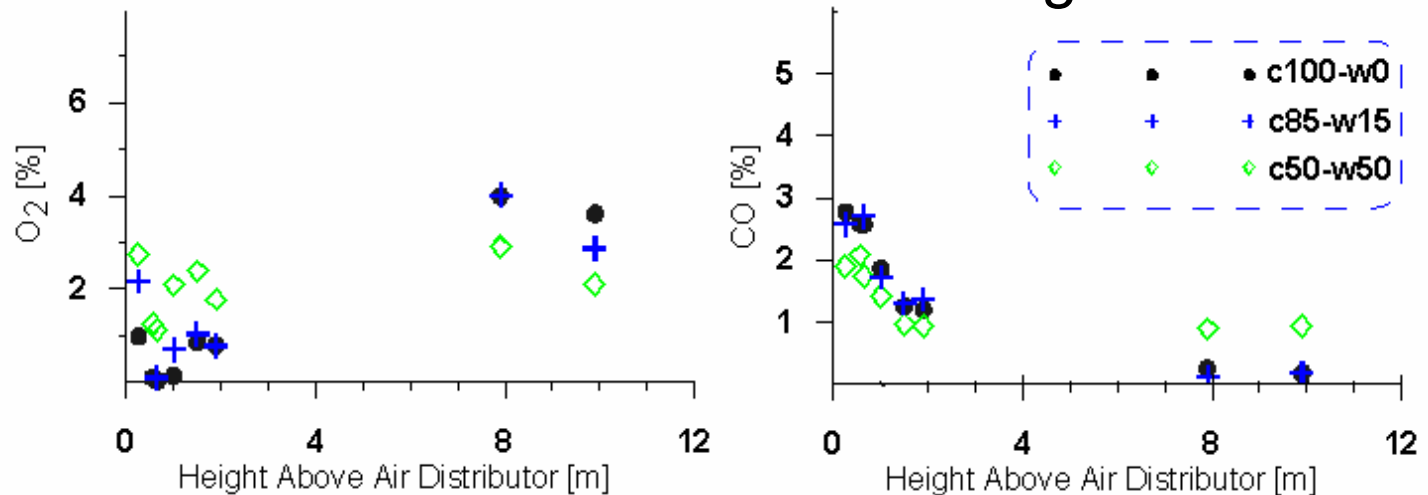


Gas mixing & combustion

Combustion kinetics are fast at typical furnace temperatures.
No coexistence of reactants.



Reactants coexist however on a time-averaged basis.

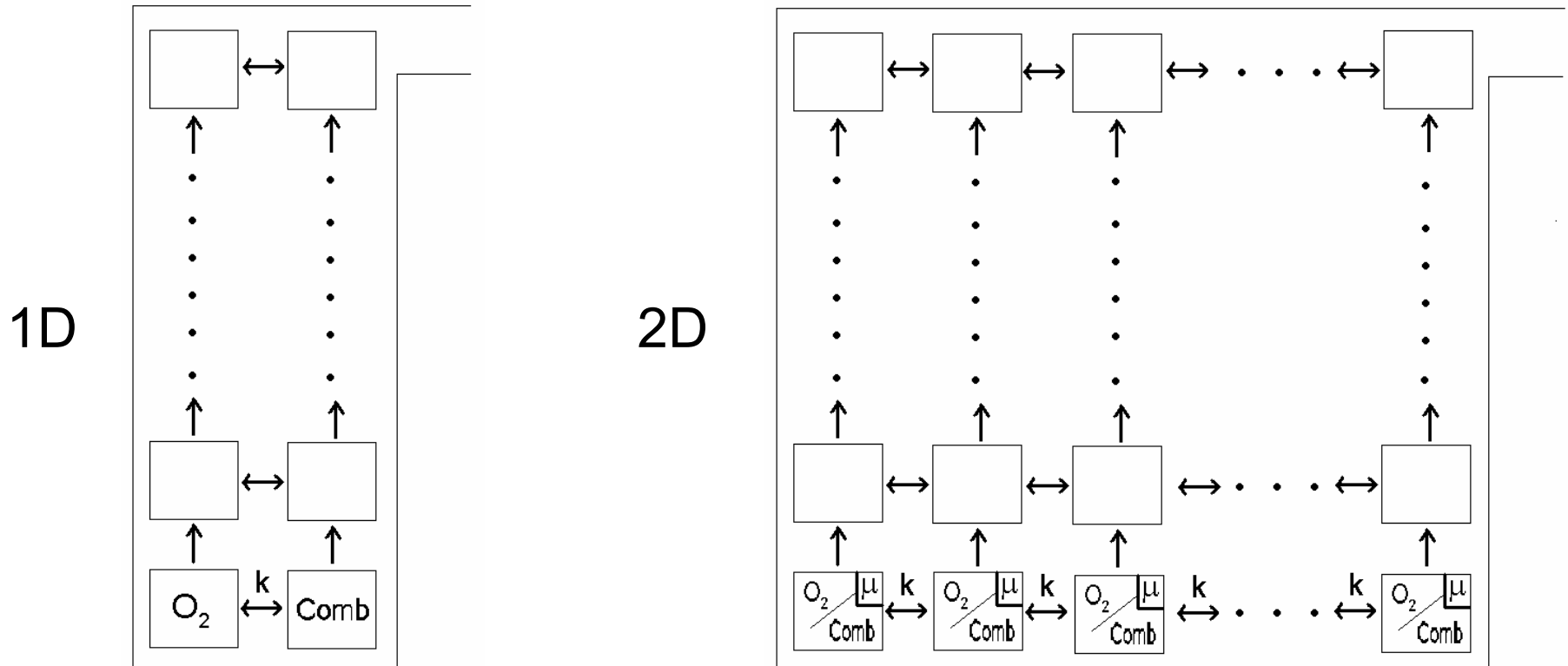


Gas mixing & combustion

Macroscopic models in literature aim at modeling the time-averaged value

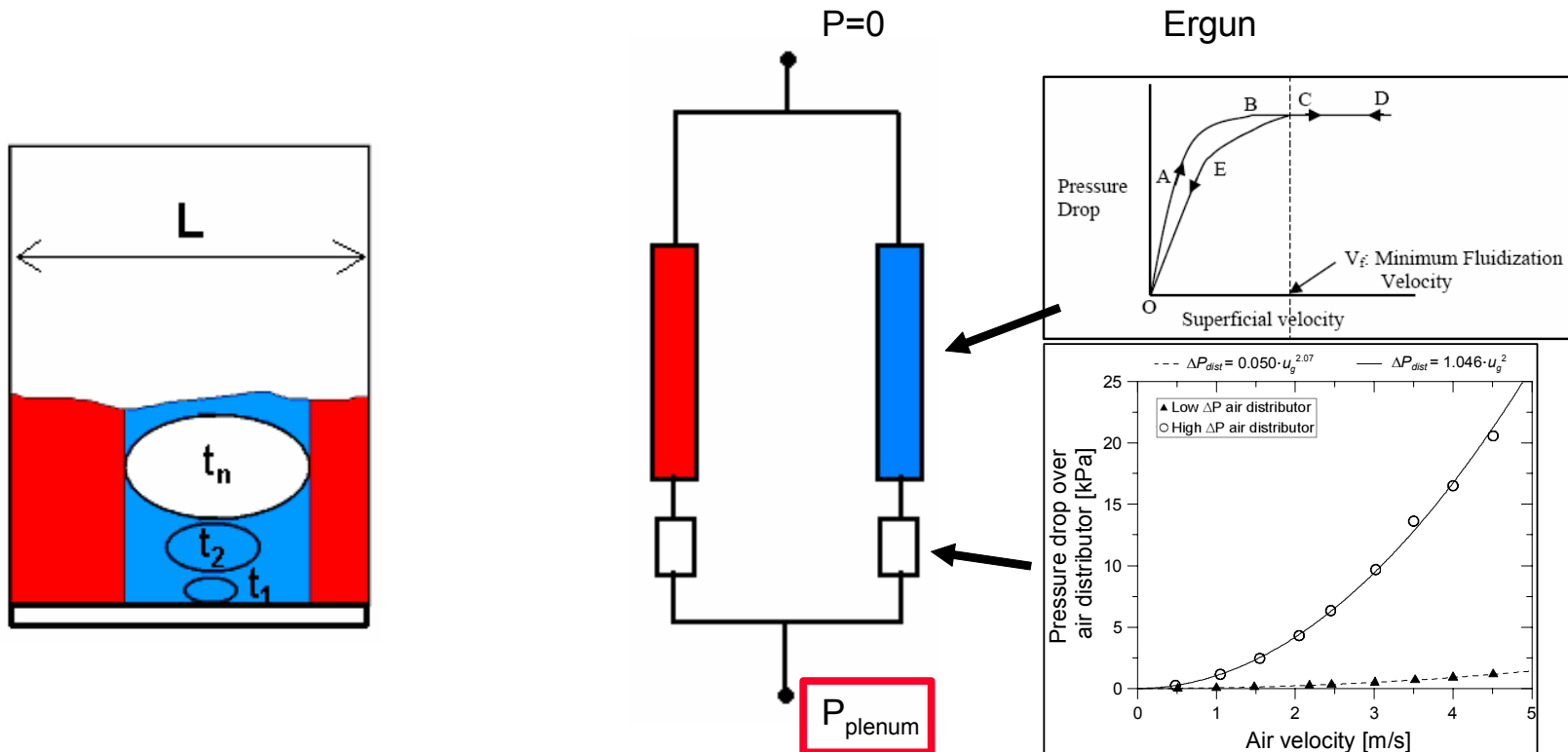


With fast combustion kinetics, a virtual mixing scale has to be used to avoid burnout and allow coexistence of reactants

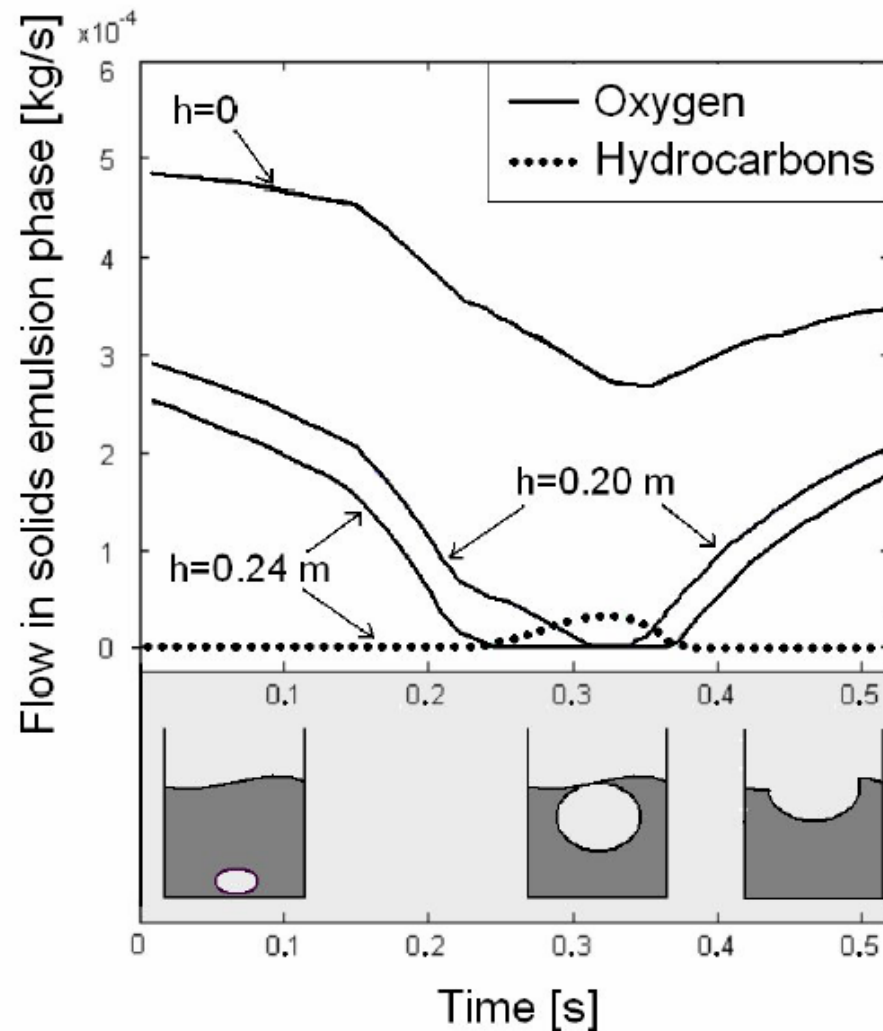


Gas mixing & combustion

Dynamical pressure balance on the gas phase

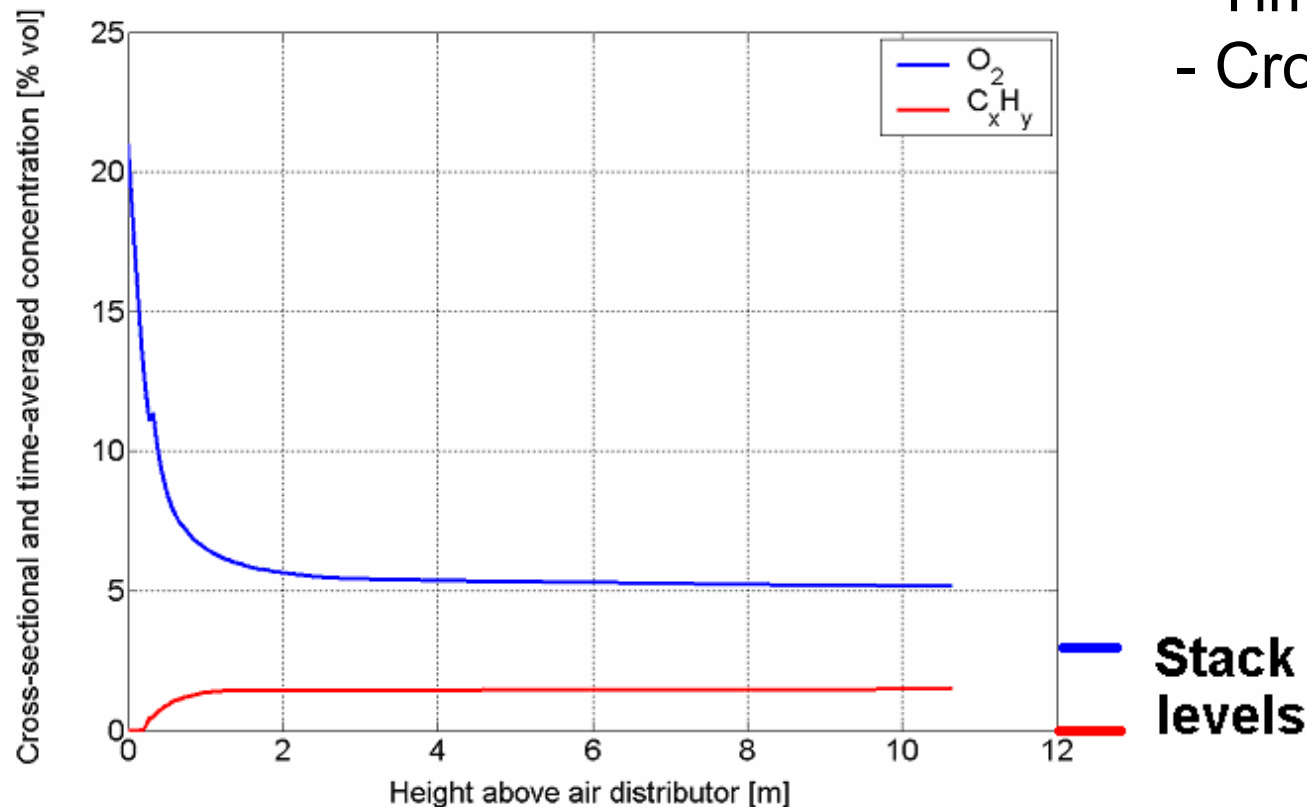


Gas mixing & combustion



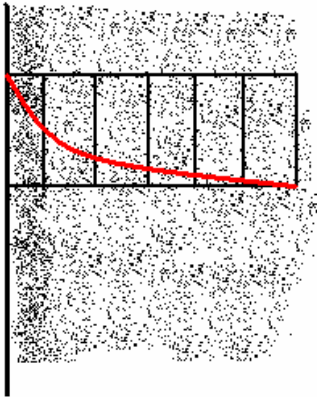
Gas mixing & combustion

Simulated data averaged in: - Gas phase
- Time
- Cross section

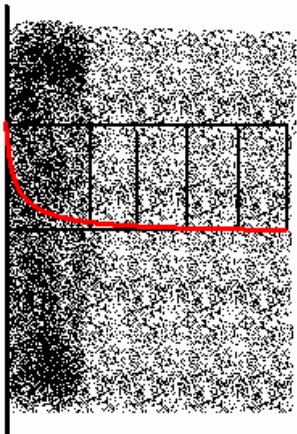


Heat balance - Radiation

Top freeboard



...



Bottom freeboard

Optical shadowing factor of a solids suspension:

$$\alpha = 1 - \exp\left(-\frac{1.5 \cdot c_v \cdot l}{d_s}\right)$$

Radiation effective T weighting for each cell:

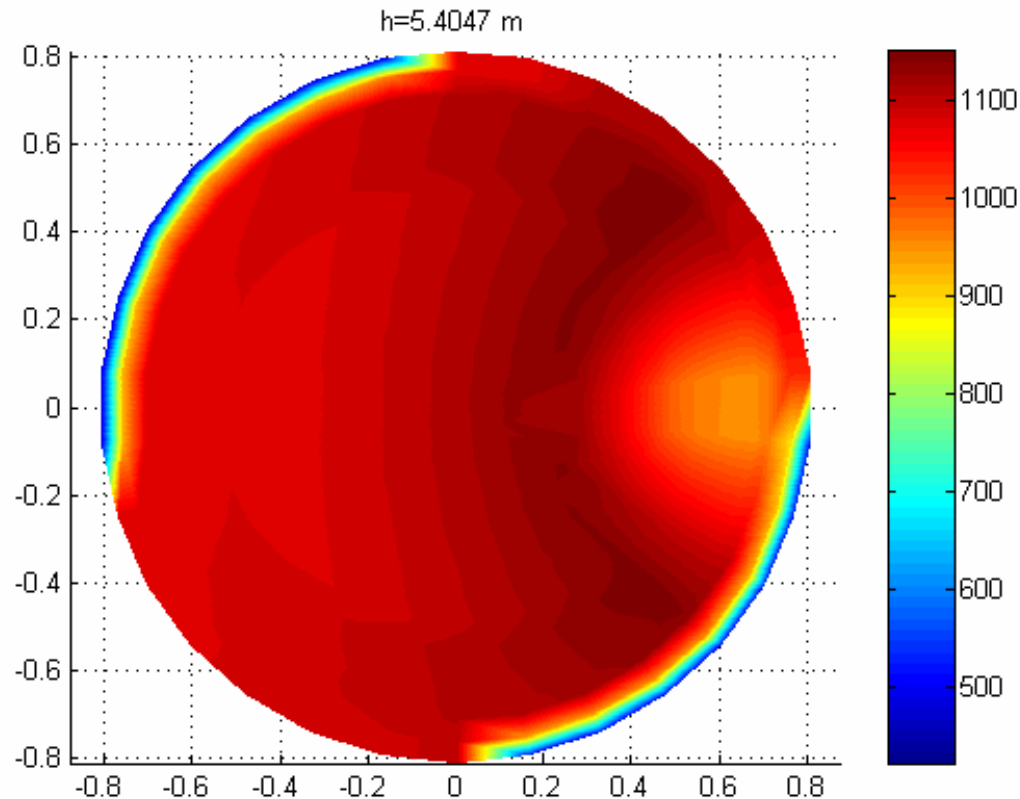
$$w_i = \alpha_i \cdot \prod_{n=1}^{n=i-1} (1 - \alpha_n) \longrightarrow \boxed{T_{eff}, C_{eff}}$$

$$\longrightarrow \boxed{Q = h_{rad} A (T_{eff} - T_{wall})}$$

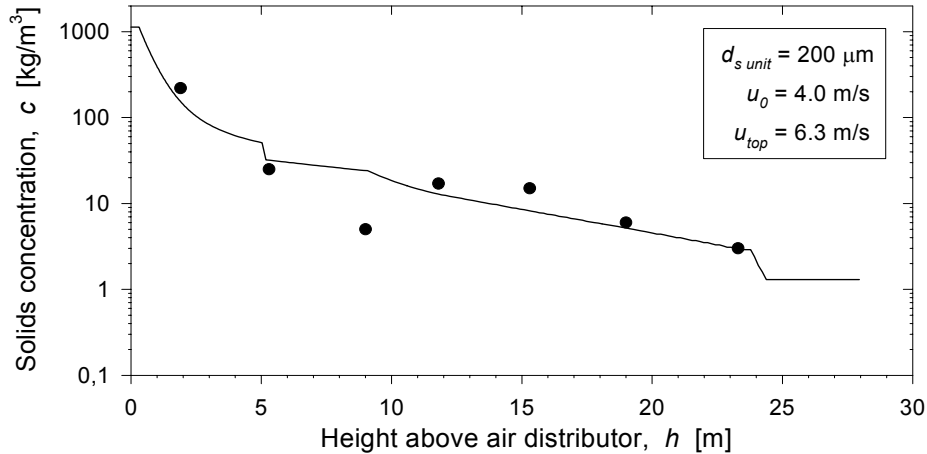
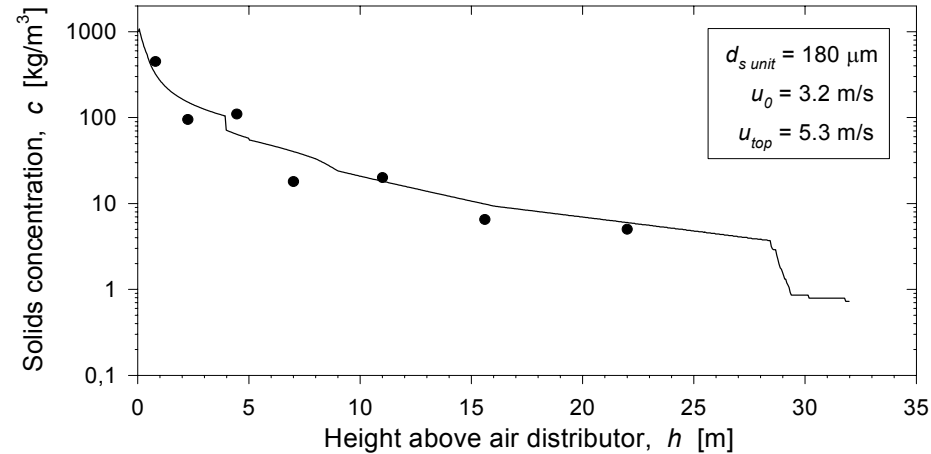
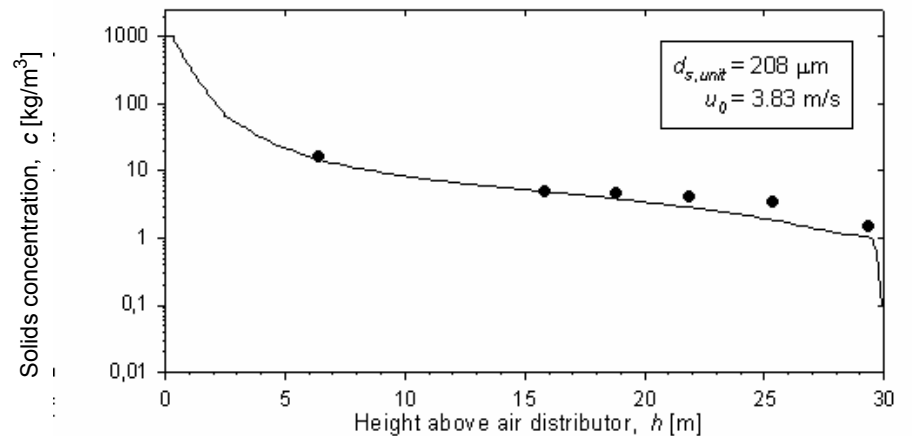
Radiation heat weighting for each cell:

$$r_i = \frac{w_i \cdot (T_i^4 - T_{wall}^4)}{\sum_{i=1}^N w_i \cdot (T_i^4 - T_{wall}^4)} \longrightarrow \boxed{Q_i = r_i Q}$$

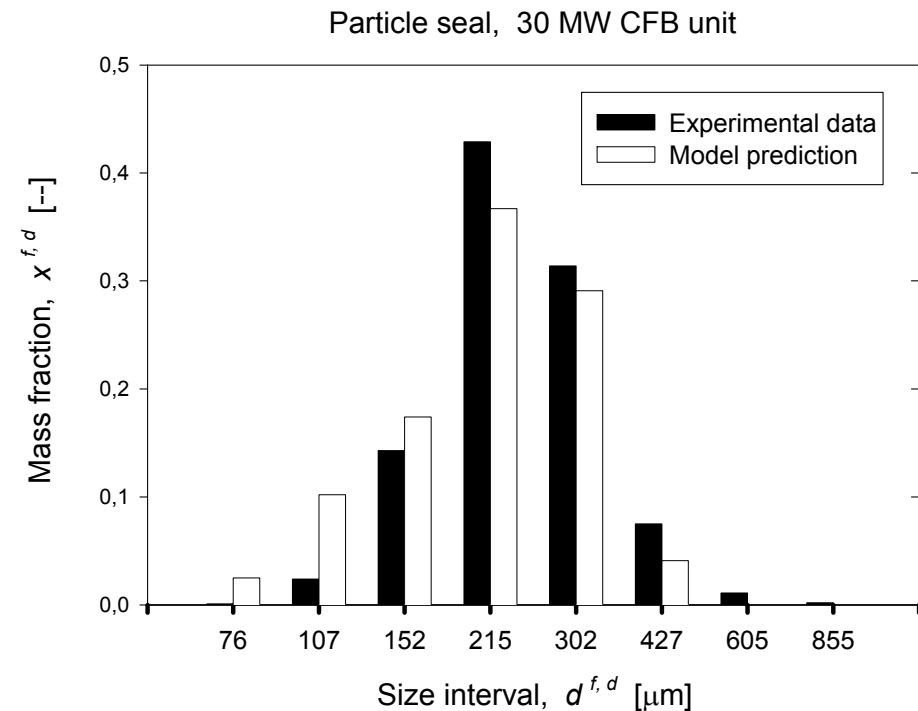
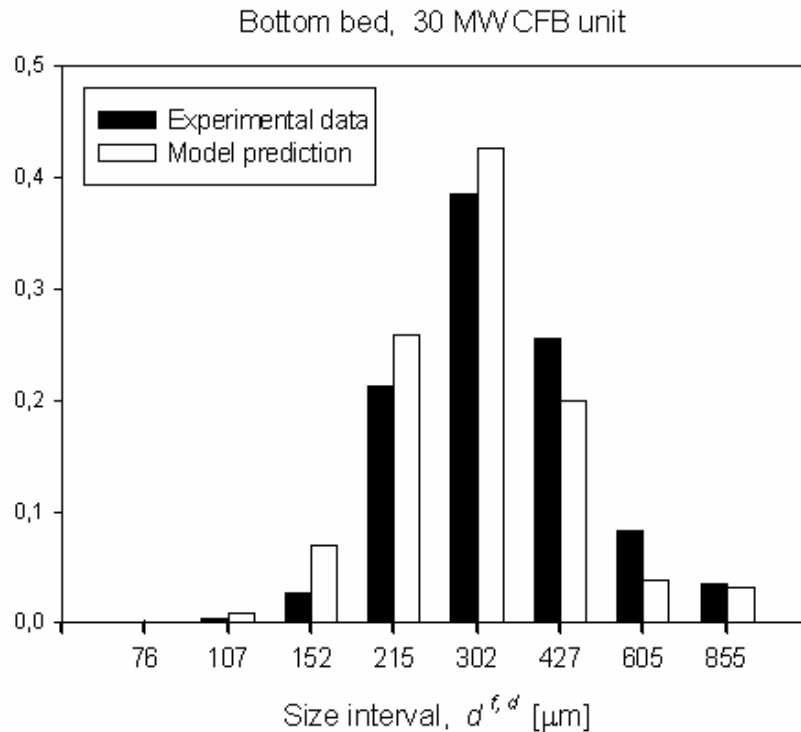
Temperature field



Solids concentration profiles

Flensburg 109 MW CFB**Duisburg 226 MW CFB****Örebro 165 MW CFB**

PSD distribution in CFB loop



Fuel concentration in dense bed

$$u_0 = 3.81 \text{ m/s}$$

$$m_{fuel} = 0.303 \text{ kg/s}$$

$$P = 9.43 \text{ MW}$$

Volatiles (wt% daf) 40.2

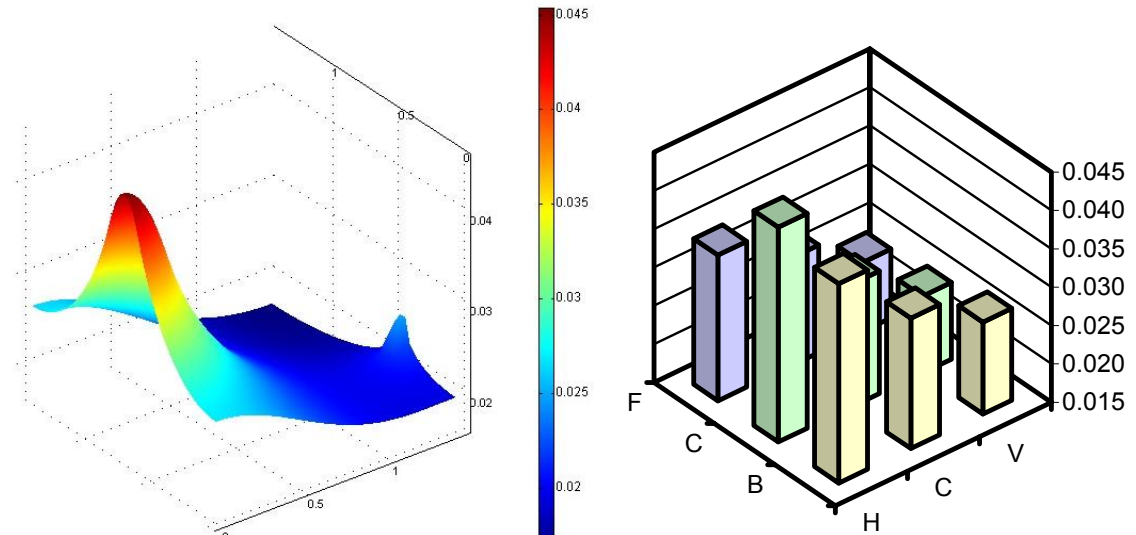
Proximate analysis (wt% a.r.)

Combustibles	74.2
Ash	8.9
Moisture	16.9

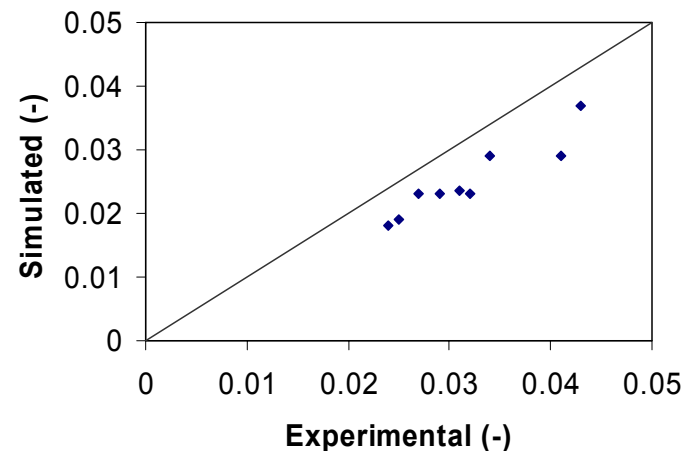
Ultimate analysis (wt% daf)

C	78.4
H	5.5
O	12.7
S	1.84
N	1.60

Heating value (MJ/kg low, daf) 31.09



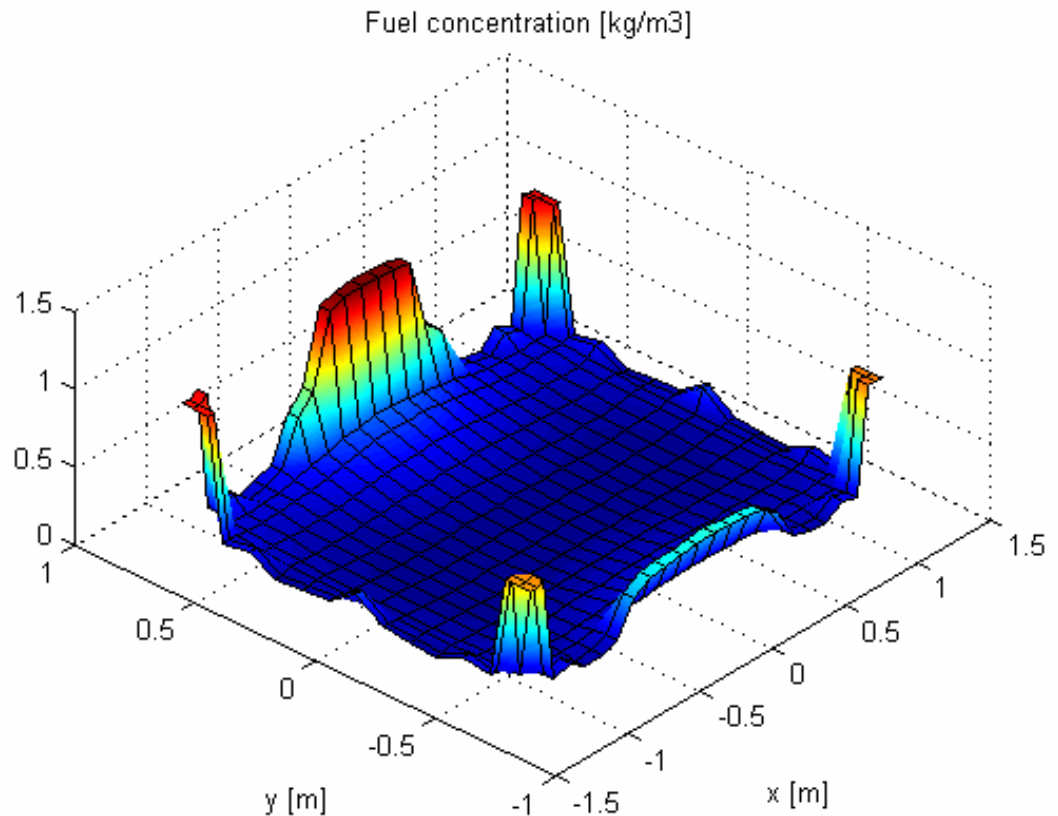
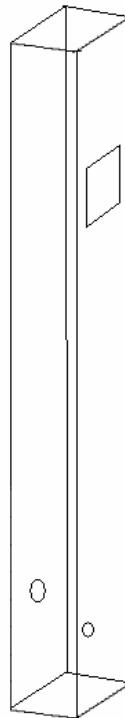
Char fraction in bottom region



Fuel concentration in freeboard

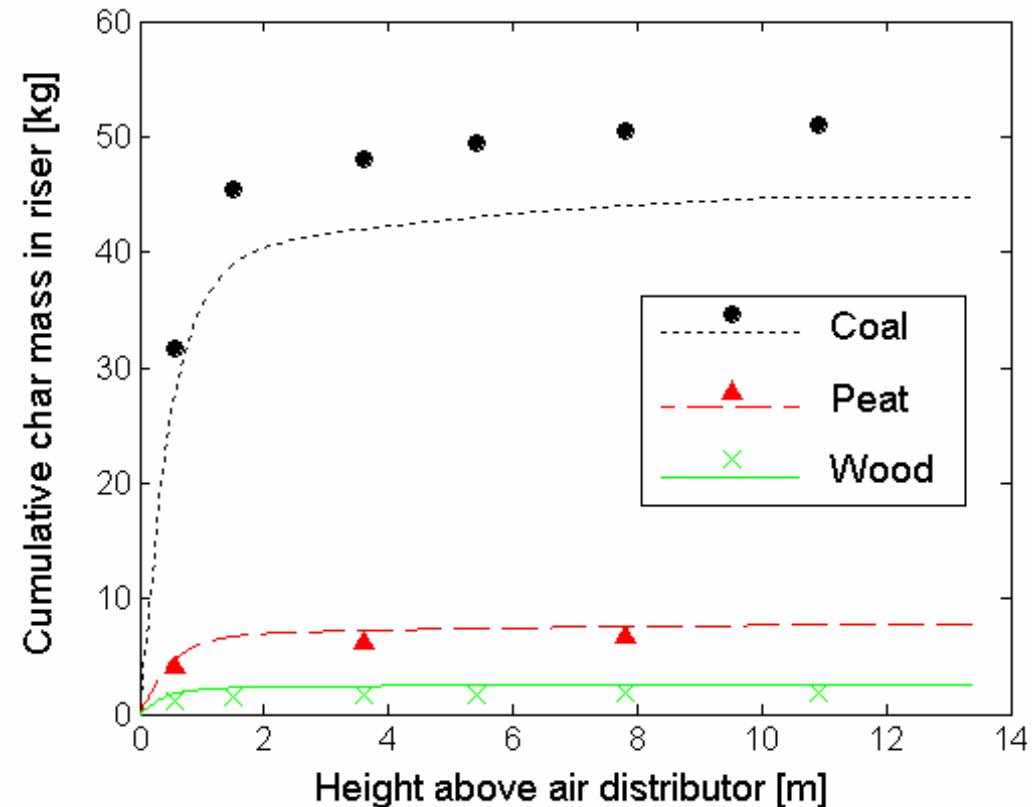
Bituminous coal

H= 7 m

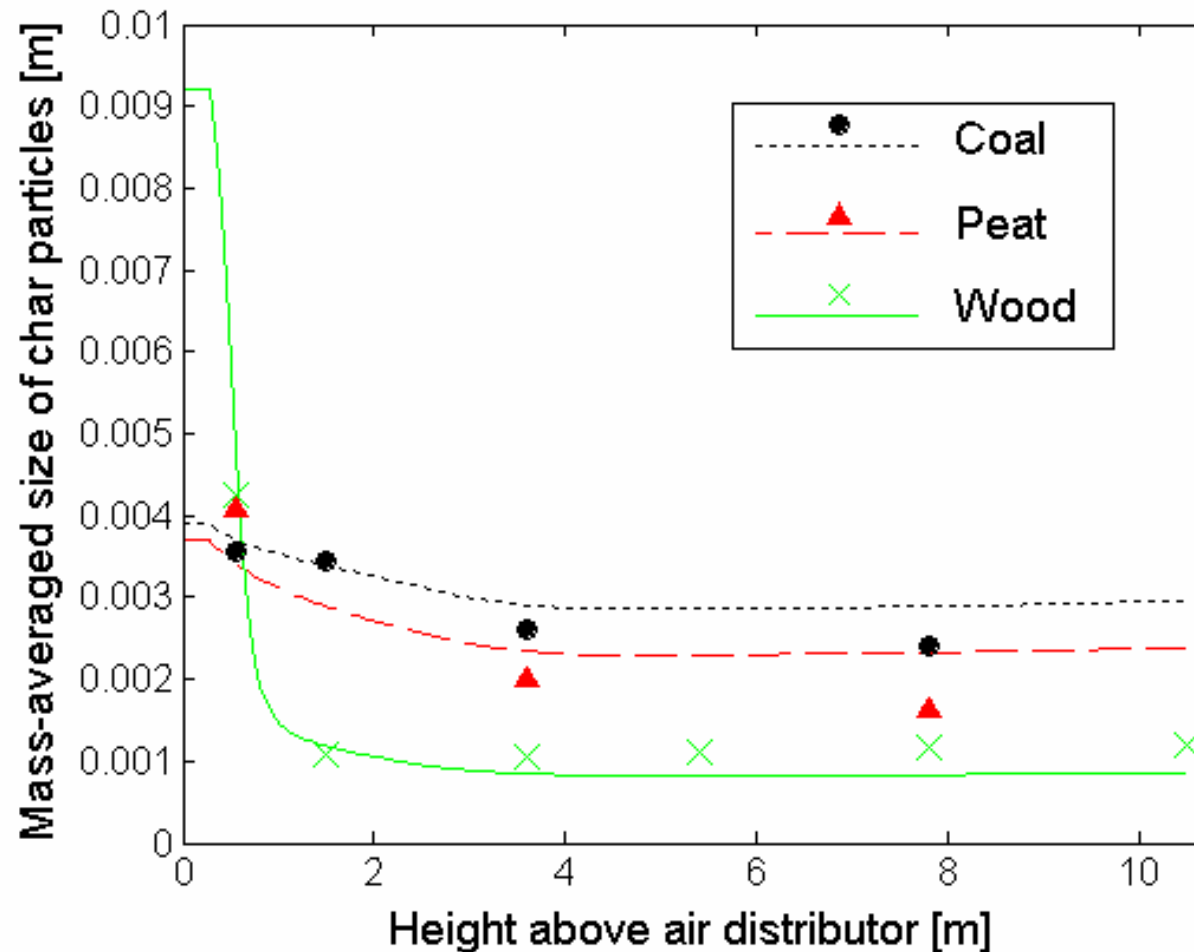


Axial distribution of char inventory

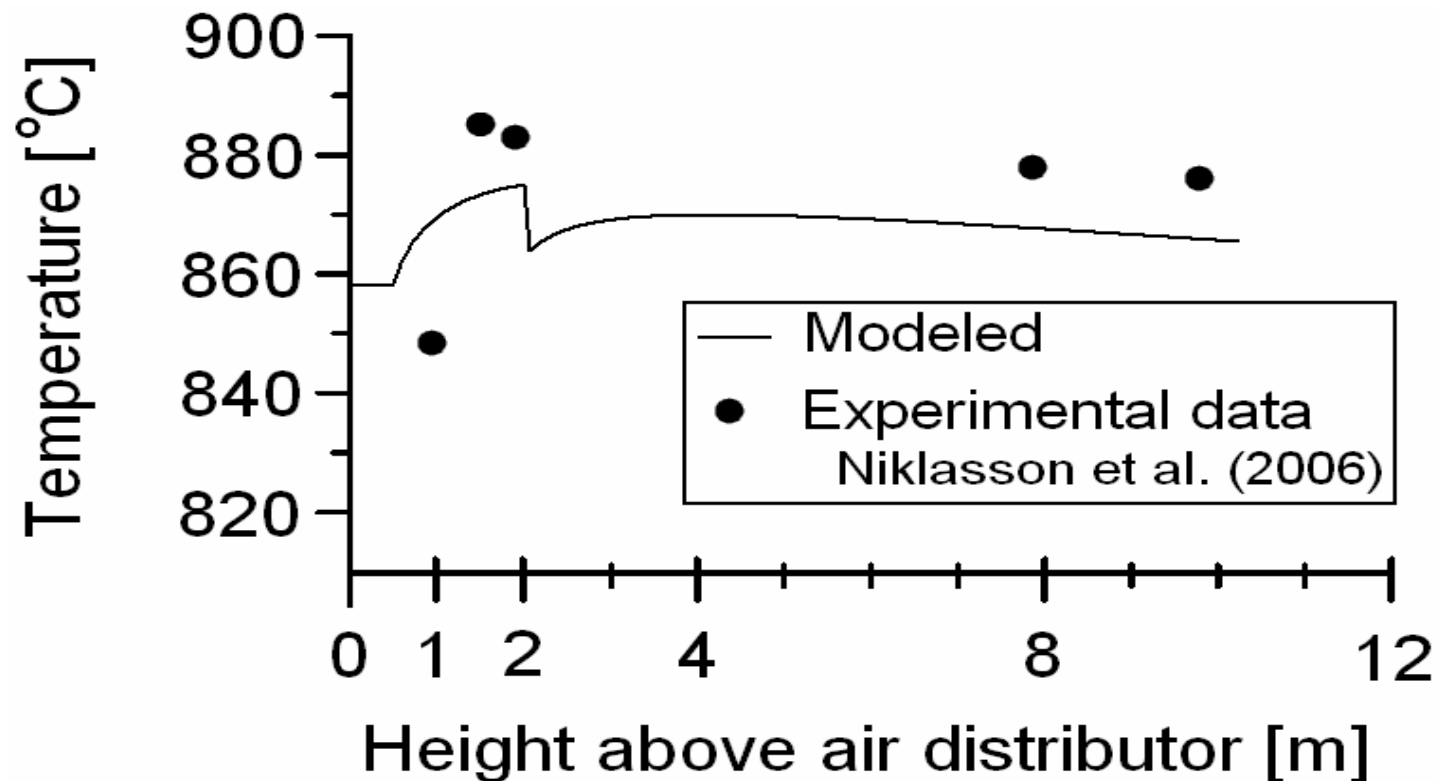
		Coal	Peat	Wood
Proximate (%)	Moisture	14.80	25.00	43.10
	Volatiles	31.36	49.97	46.10
	Char	47.24	22.03	10.40
	Ash	6.60	3.00	0.40
Ultimate daf (%)	C	79.8	59.5	50.6
	O	12.6	31.5	43.2
	H	5.3	6.4	5.9
	N	1.56	2.1	0.22
	S	0.72	0.53	0.04
LHV [MJ/kg ar]		29.0	20.8	17.6



Axial distribution of fuel size



Temperature profile

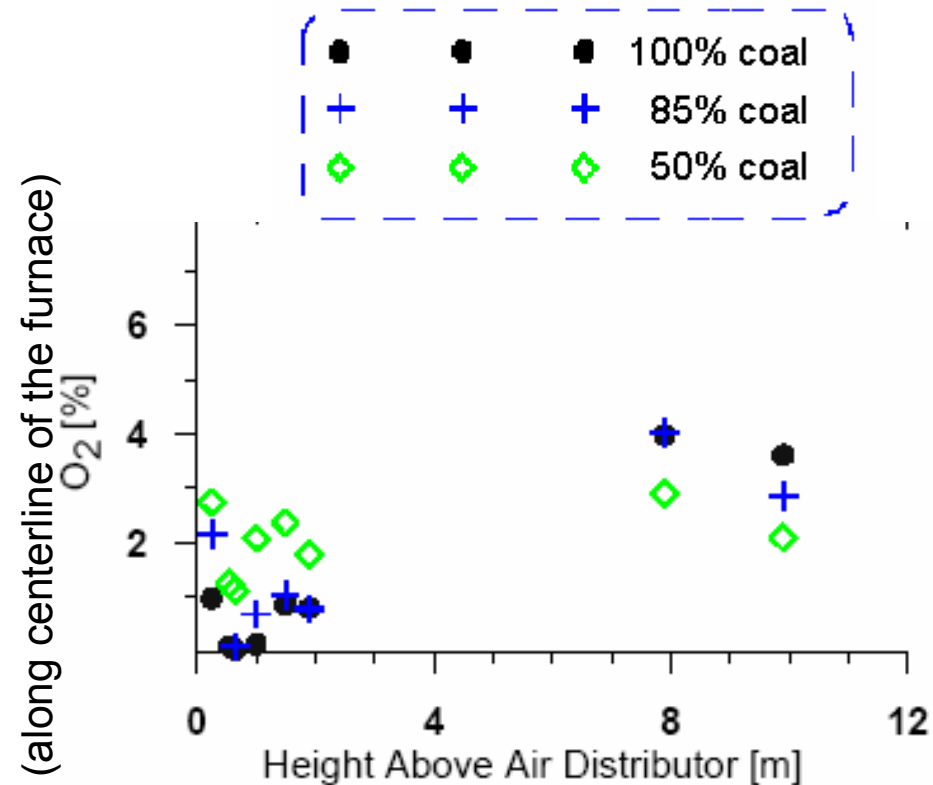


Gas probes in CFB units

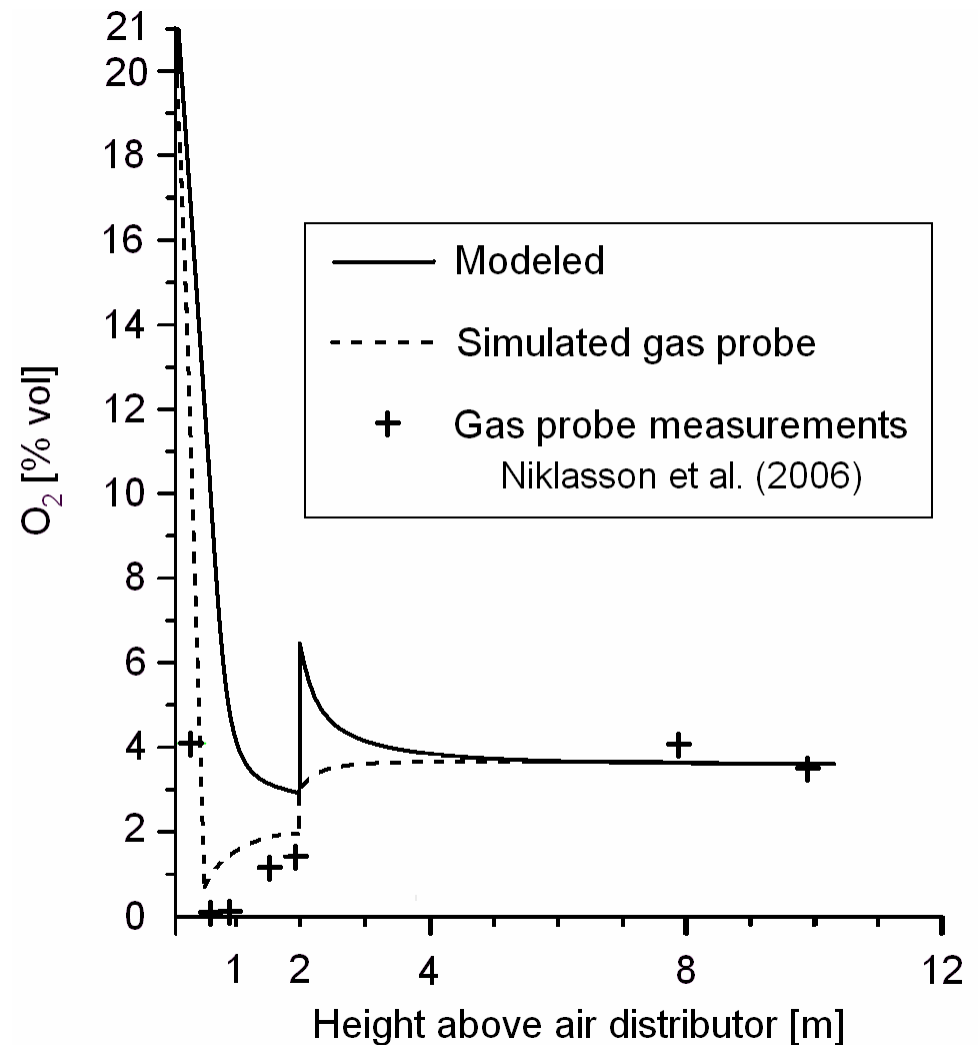
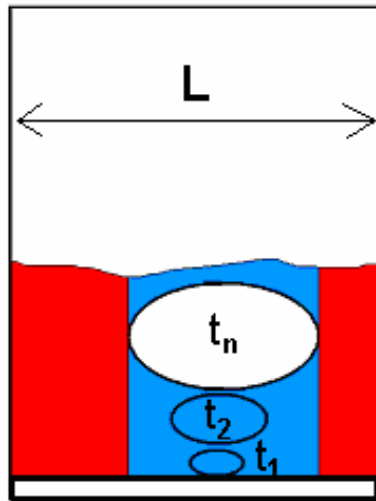


High-velocity oxidizing gas phase
&

Low velocity reducing gas phase



Gas probe simulation



Further work

- Model steady-state PSD of bed material
- Enable several inert solid fractions
- Enable several fuel fractions
- Include kinetically-controlled reactions
- Include heterogeneous reactions

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