

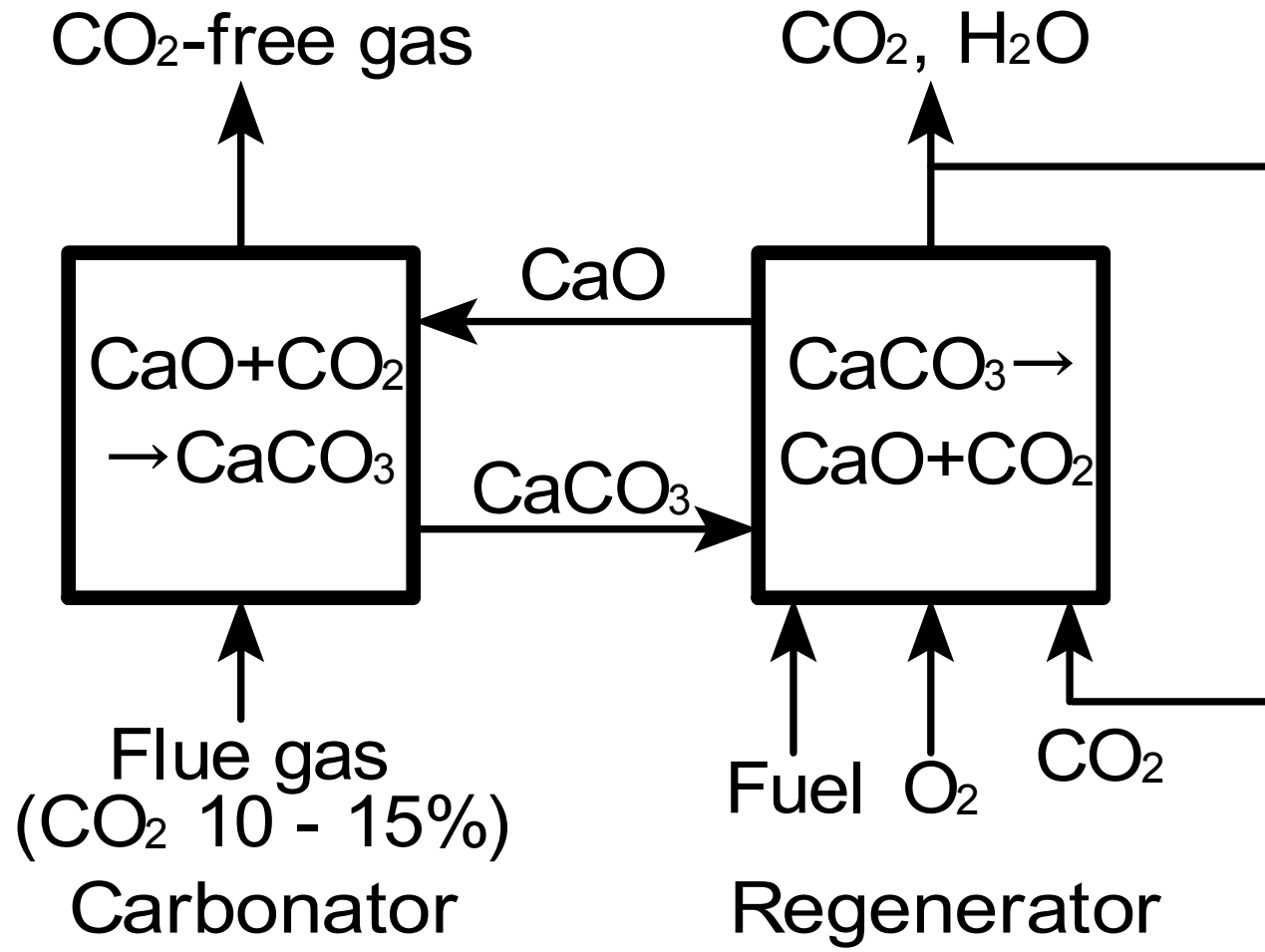
# **N<sub>2</sub>O Decomposition by CaO under Conditions of Carbonator of Calcium Looping Cycle**



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# Principle of CaL process for CO<sub>2</sub> separation

CaL process consists of a carbonator and a regenerator. In the carbonator, flue gas from air-blown combustor is introduced. In the regenerator, **fuel** (coal) is burned to supply heat to decompose CaCO<sub>3</sub> to CaO.



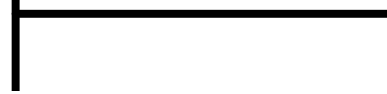
# Flue gas from air-blown FB combustor

CaL process consists of a carbonator (absorber) and a regenerator. In the regenerator, **fuel** (coal) is burned to supply heat to decompose  $\text{CaCO}_3$  to  $\text{CaO}$ .

$\text{CO}_2$ -free gas



$\text{CO}_2, \text{H}_2\text{O}$



# Flue gas from

# contains N

# Char transportation from regenerator to carbonator

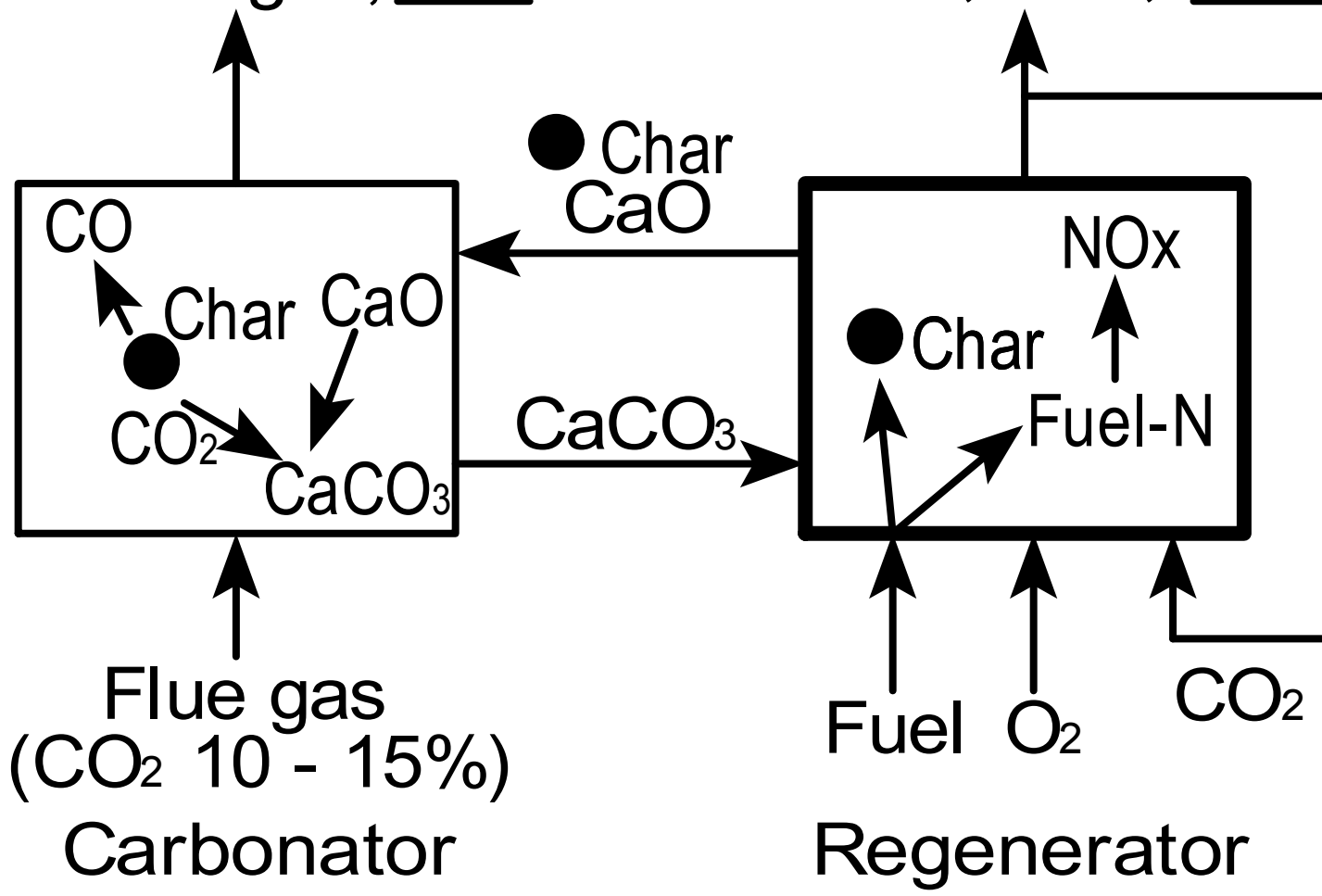
Coal combustion in regenerator.

→ Formation of char and transportation of char with CaO

→ Formation of CO and/or CO<sub>2</sub>

CO<sub>2</sub>-free gas, CO

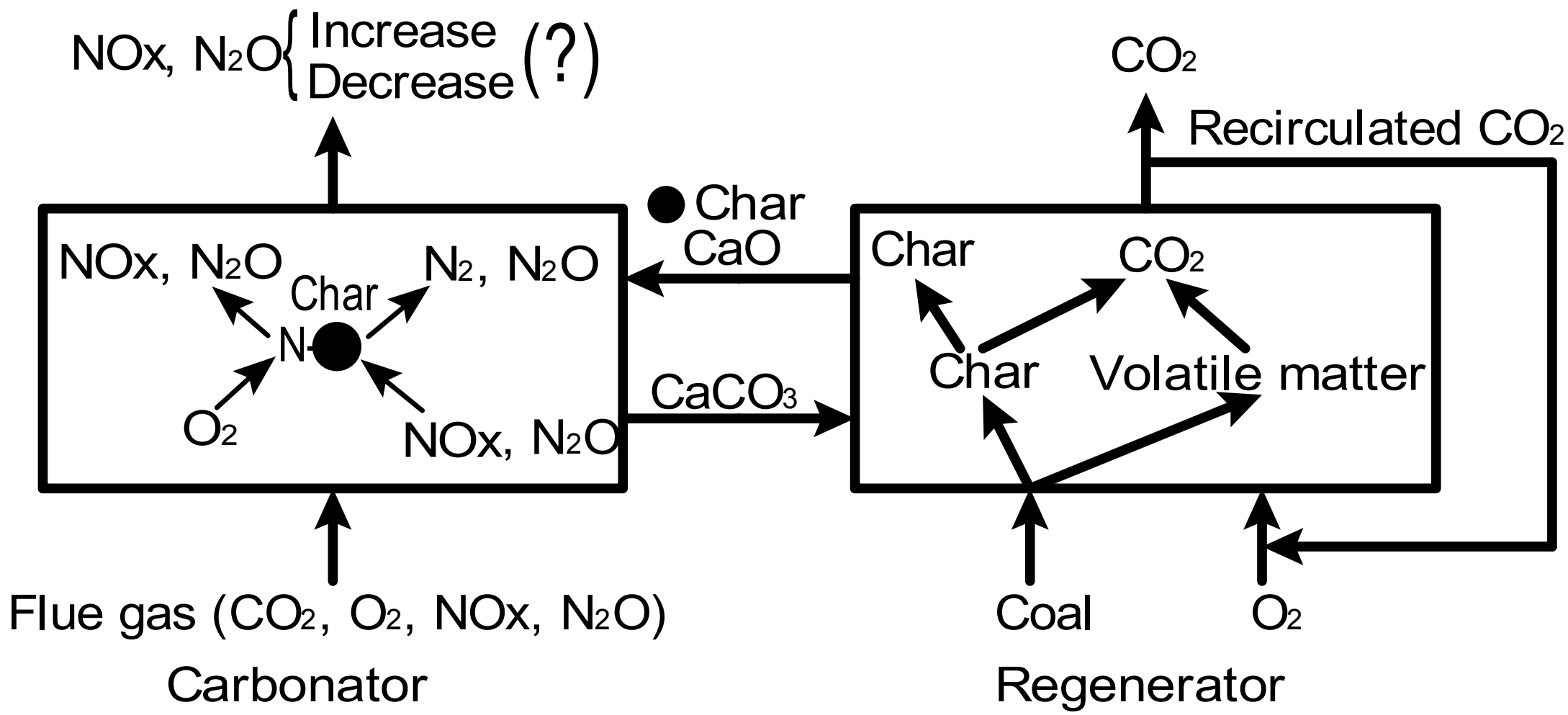
CO<sub>2</sub>, H<sub>2</sub>O, NOx



# Possible roles of char in carbonator

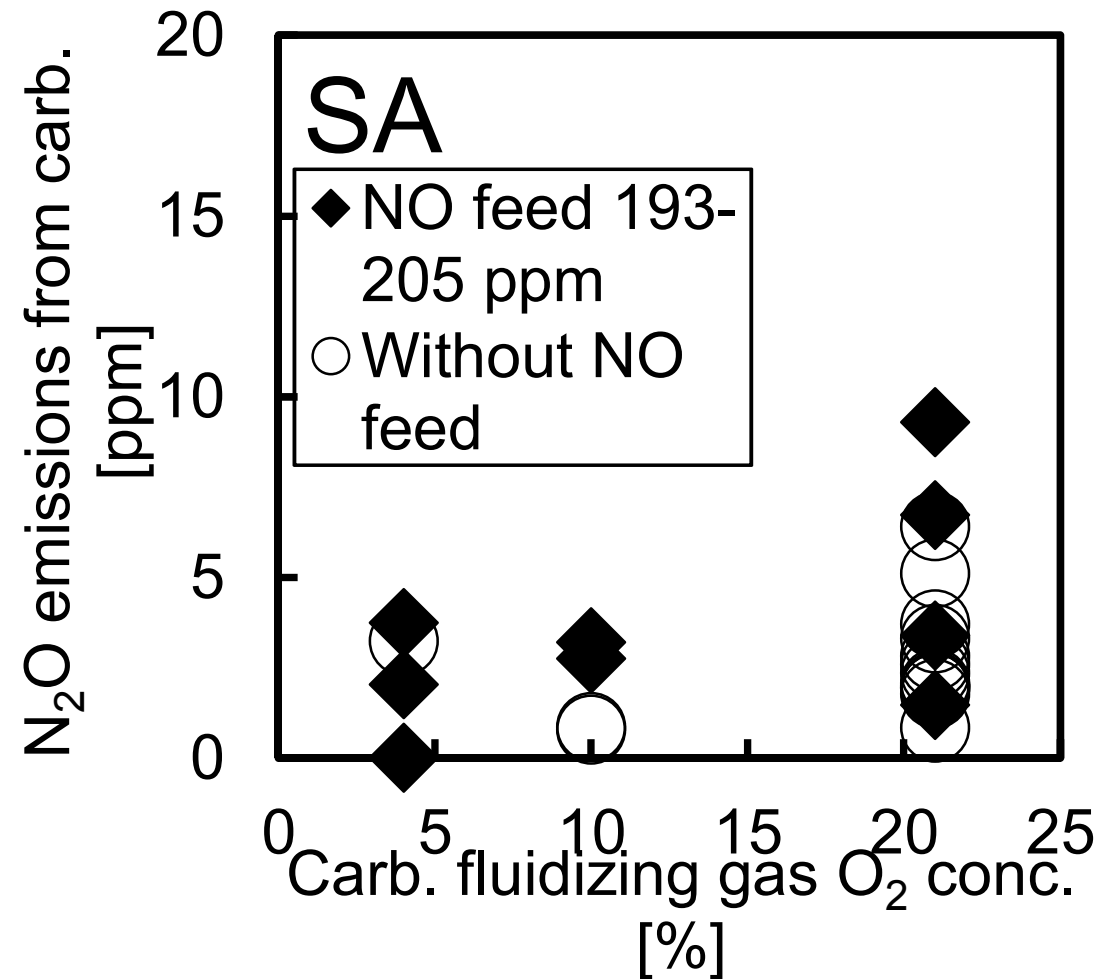
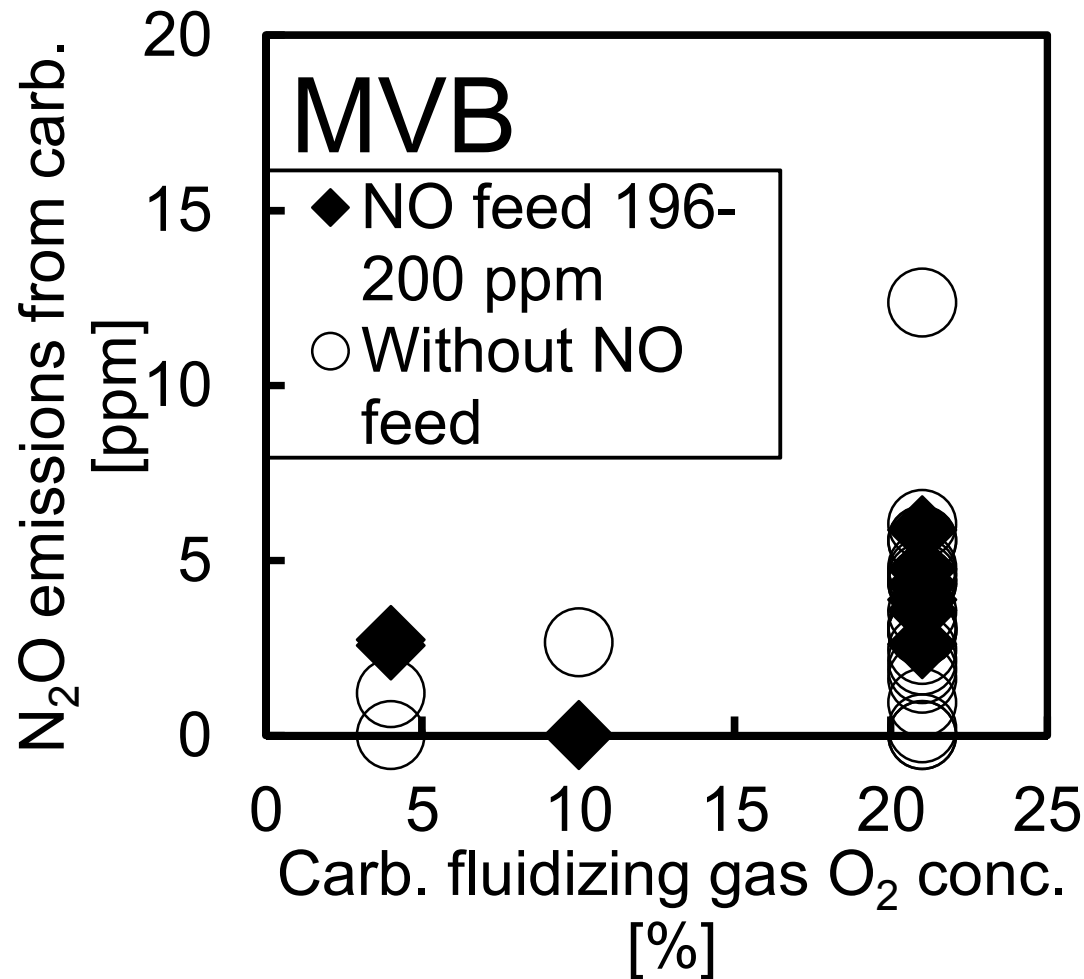
Char is expected to have different roles in carbonator:

- Oxidation of char-N : formation of  $N_2O$
- $C+N_2O \rightarrow N_2$ :  $N_2O$  reduction



# N<sub>2</sub>O formation from char oxidation/NO reduction

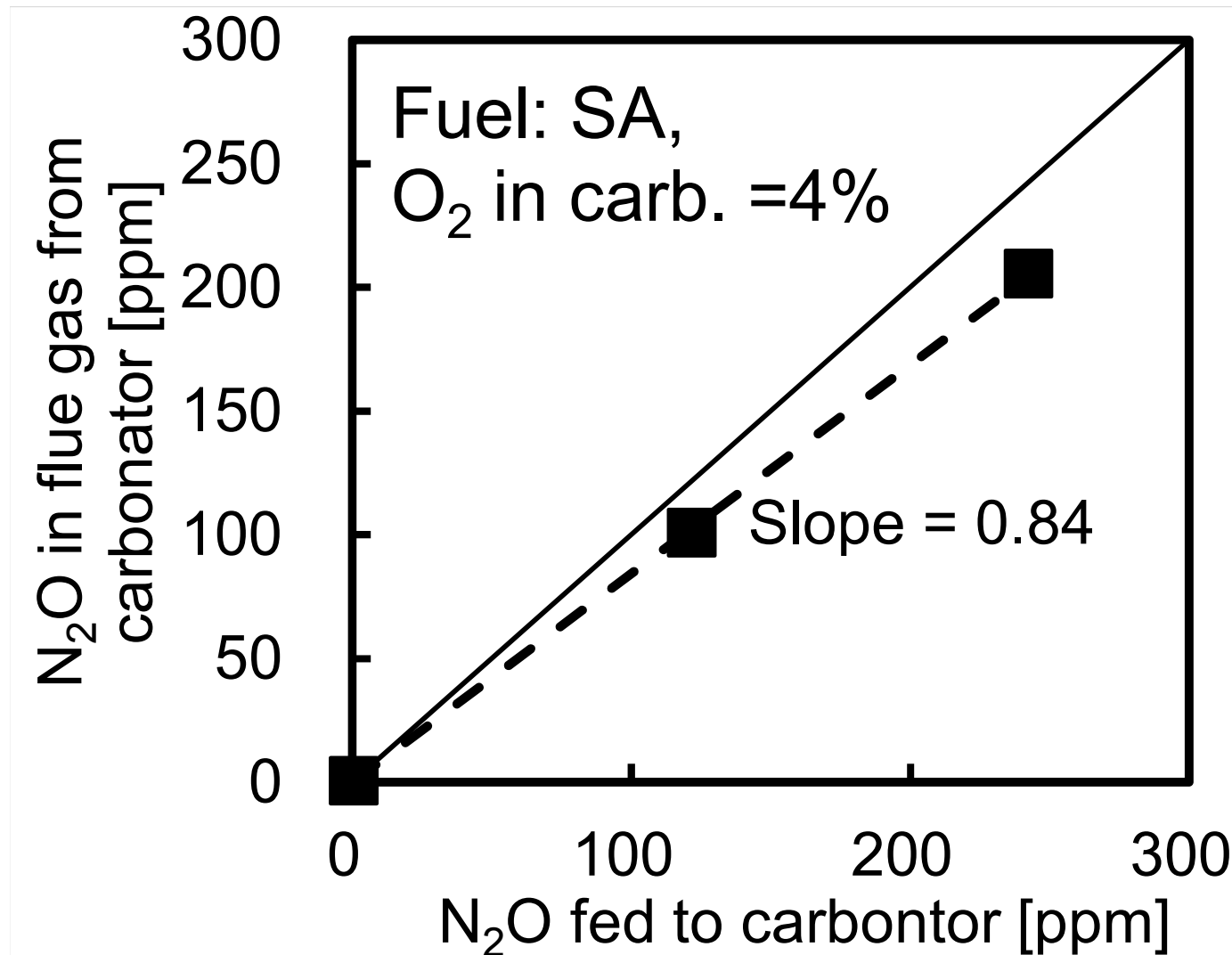
N<sub>2</sub>O emissions from char combustion / NO reduction by char were only slight (<10 ppm = 0.3% CO<sub>2</sub>-equivalent).



(Shimizu et al., J. Jpn. Inst. Energy, 94, 841-850, 2015)

# Reduction of fed $N_2O$ in carbonator

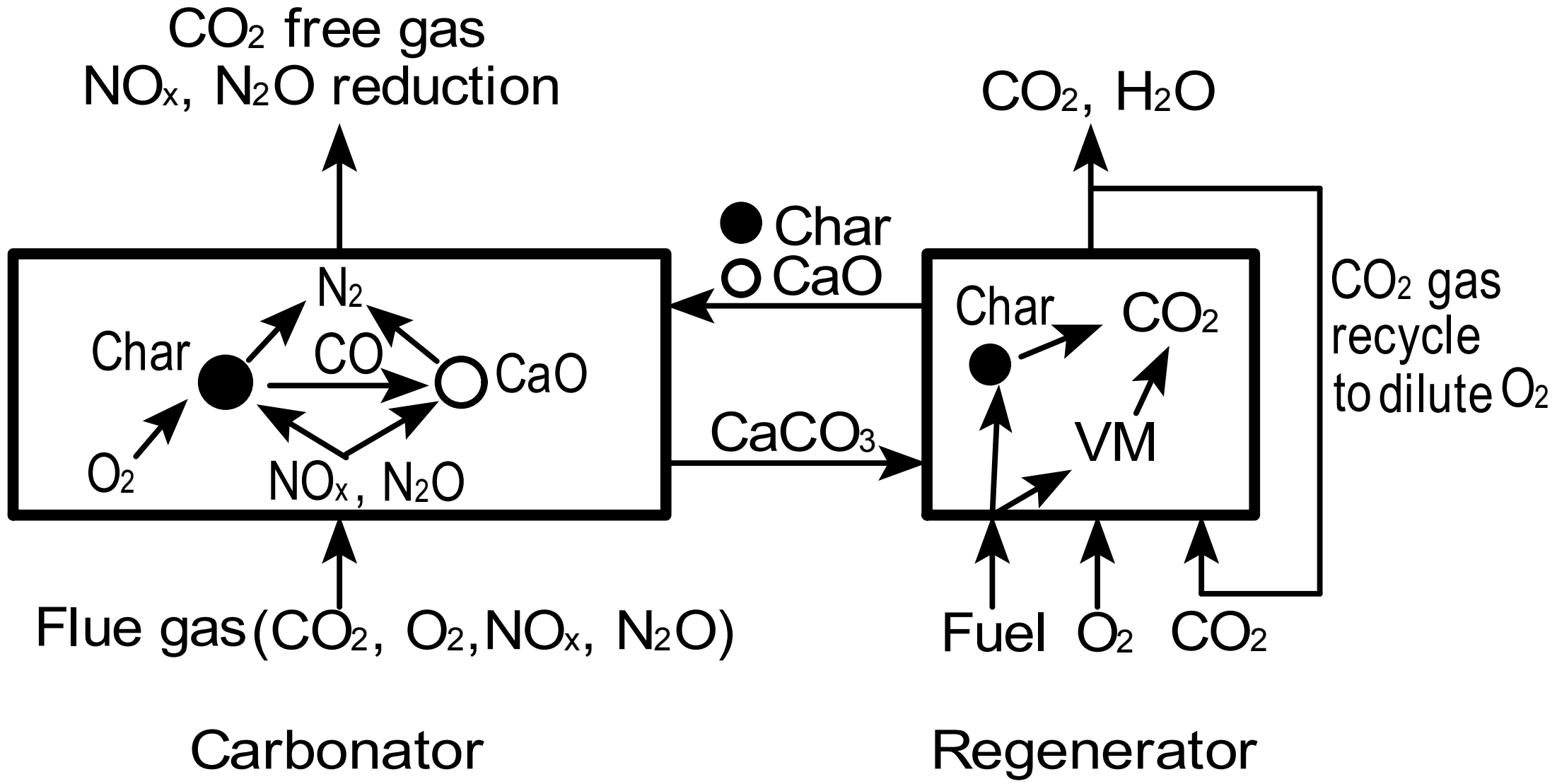
For semi-anthracite, about 16% of  $N_2O$  in fluidizing gas was reduced in carbonator.



(Shimizu et al., 6<sup>th</sup> HTSLC Meeting (Milan, Italy, 2015))

# Expected N<sub>2</sub>O reduction by CaO in carbonator

CaO is expected to catalyze N<sub>2</sub>O decomposition and reduction by CO which is formed by char oxidation.



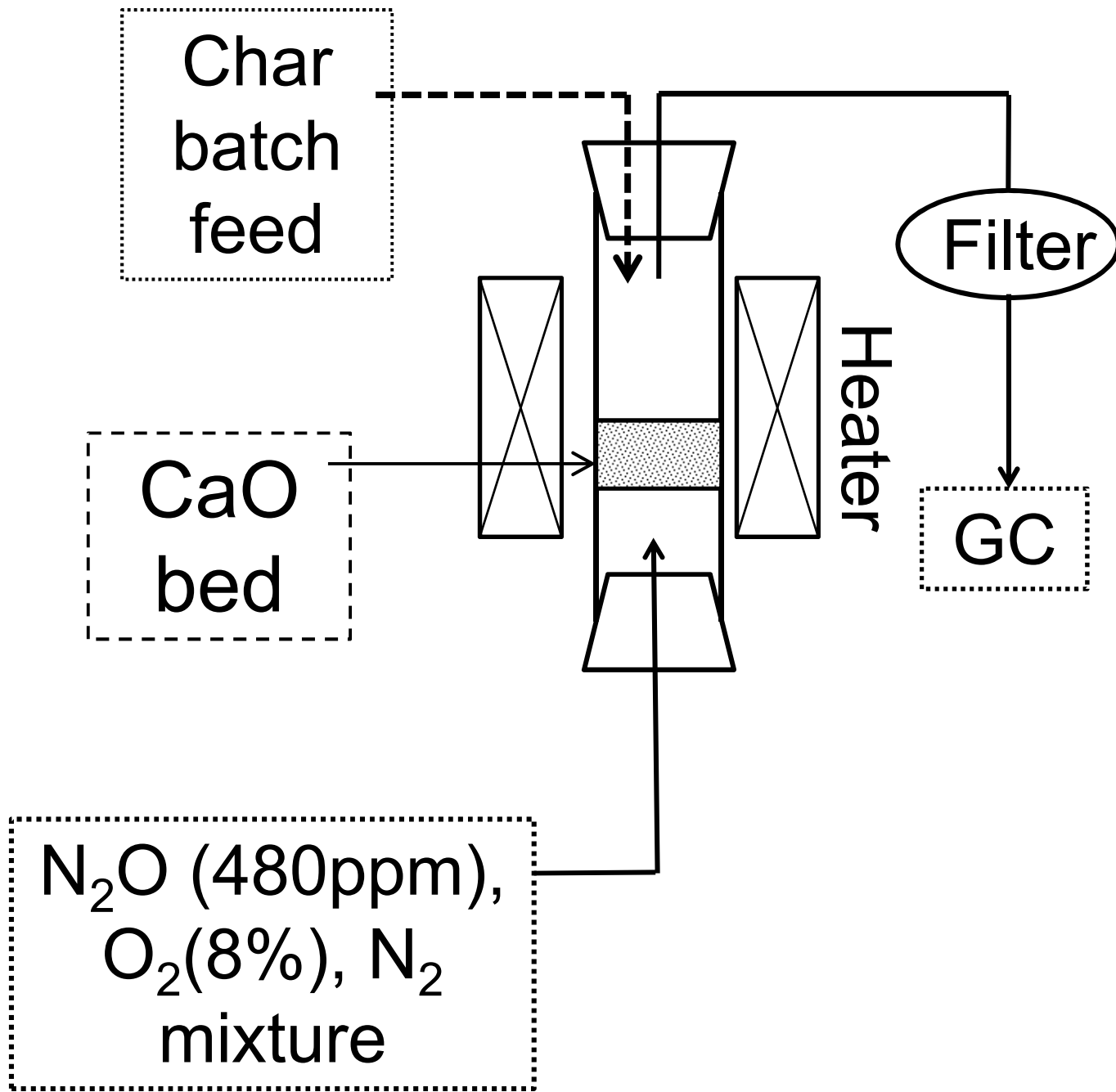


# This work

## Basic study on N<sub>2</sub>O decomposition by CaO using quartz FB reactor

N<sub>2</sub>O-containing gas was fed to a bubbling fluidized bed of CaO at 600 °C to evaluate N<sub>2</sub>O decomposition. Also batch feed of char to the CaO bed was conducted.

# Experimental apparatus



Quartz FB

ID 26mm

Limestone (0.35-0.42 mm) calcined at 900 °C

Static bed height

$H_s = 7$  cm

Temp. 600 °C

$U_{\text{gas}} = 17$  cm/s

( $H_s/U_{\text{gas}} = 0.4$  s)

## Char batch feed

Char was prepared by heating at 900 °C in N<sub>2</sub>.  
Batch feed was conducted.

### Analyses of char

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Ash (dry)	Moist. (sample)	C (daf)	H(daf)	N(daf)
23.3	2.0 - 3.5	95.8	0.6	1.2

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VM content: 2 - 3% of combustible part. (TGA weight loss in N<sub>2</sub> between 200 – 600 °C)

# Results and Discussion

- $\text{N}_2\text{O}$  decomposition by  $\text{CaO}$  without char
- Char batch feed to  $\text{CaO}$ /inert bed

# N<sub>2</sub>O decomposition without char feed

Silica sand bed: nearly 0% conversion  
(no thermal decomposition at 600 °C)

CaO bed: **nearly 100% decomposition**  
(480ppm at inlet → <1 ppm at outlet)

$$k\tau = \ln(\text{In}/\text{Out}) > 6.2^*$$

$k$ : first-order rate constant :[1/s]

$\tau$ : contact time [s]

(\*: This value includes bubble-emulsion mass transfer resistance)

# Rate of N<sub>2</sub>O reduction by CaO

In **dry** gas, rate expression is:

$$k_{\text{N}_2\text{O}}(0) = 2.8 \times 10^7 \exp(-1.057 \times 10^4 / T) = 154 \text{ [1/s]}.$$

(Shimizu et al., Energy Fuels 2000, 14, 104-111)

Gas-solid contact time:  $\tau = 0.2 \text{ s}$

$$\rightarrow k_{\text{N}_2\text{O}} \tau = 30$$

→ Contribution to N<sub>2</sub>O reduction.

# N<sub>2</sub>O decomposition by CaO in the presence of H<sub>2</sub>O

In the presence of water, rate expression is:

$$k_{N_2O} = \frac{k_1}{1 + K_1 P_{H_2O}} + \frac{k_2}{1 + K_2 P_{H_2O}}$$

(Shimizu et al., Energy Fuels

$$k_{N_2O}(0) = k_1 + k_2 \quad (0.2000, 0.4000, 0.4111) \quad T = 0.685$$

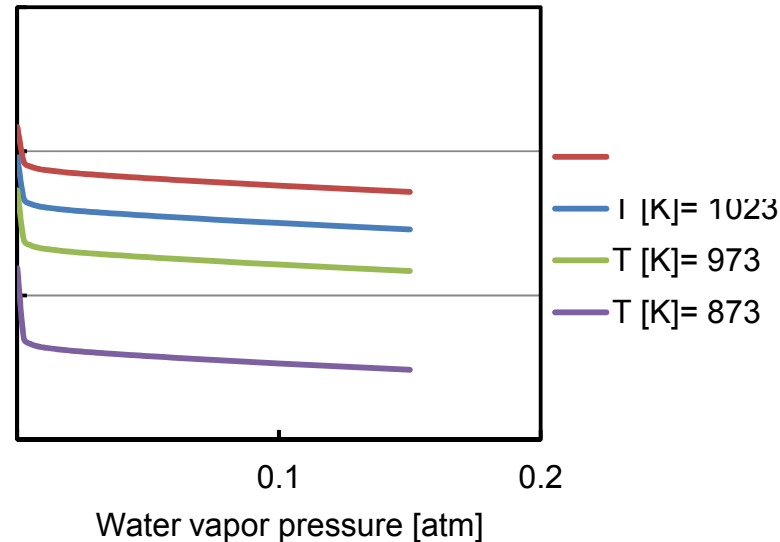
$$k_{N_2O}(0) =$$

$$K_1 = 43 \exp$$

At 600 °C and  
and  $P_{H_2O} = 0.1$

$$k_{N_2O} = 34 \text{ s}^{-1}$$

→ Contribution to  
N<sub>2</sub>O reduction is  
expected.



## Char batch feed to CaO bed

During the experiments, char batch feed (40 – 50 mg) was conducted. Formation of CO, CO<sub>2</sub> and change in N<sub>2</sub>O were observed.

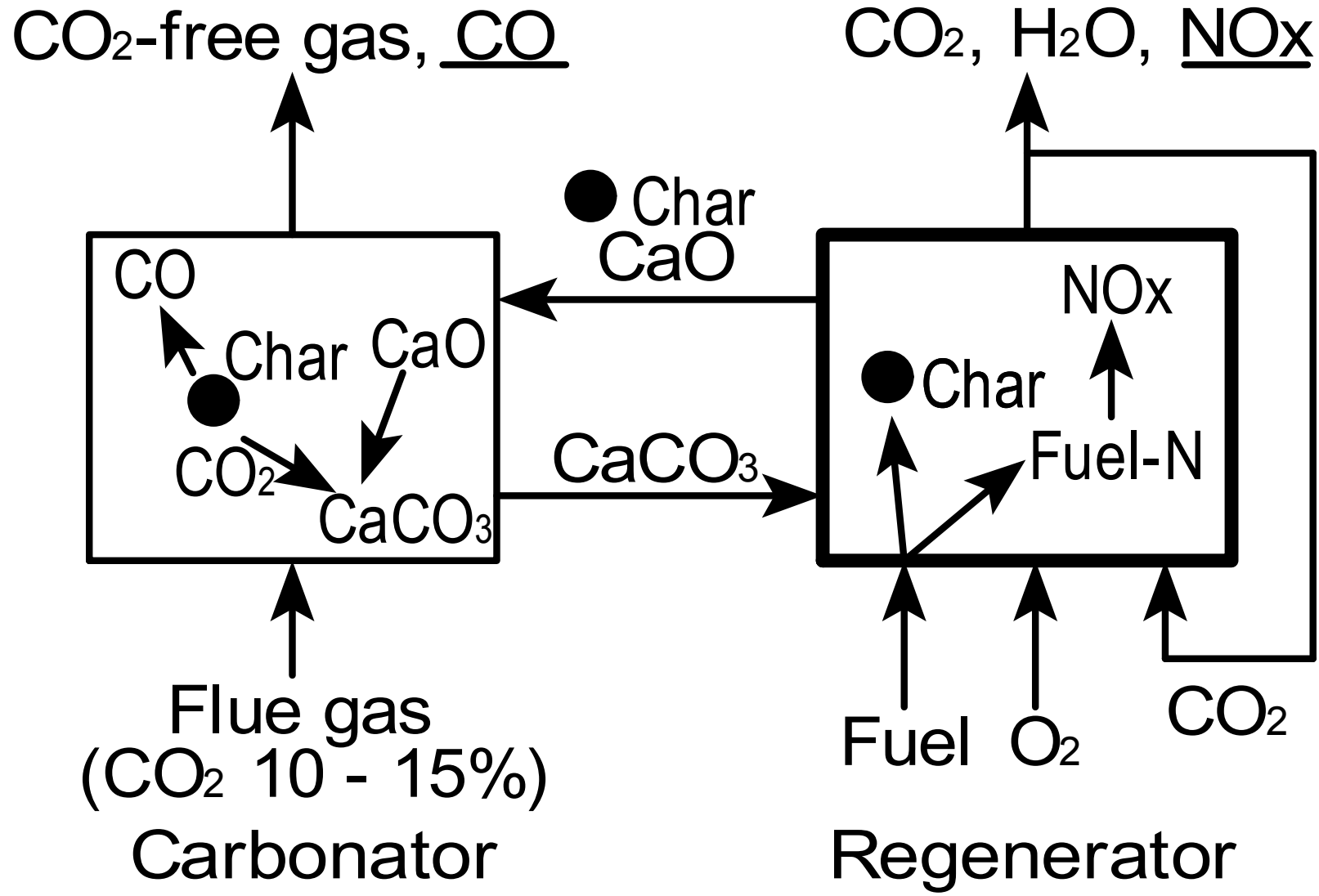
Under the present condition, however, the effect of char feed on N<sub>2</sub>O decomposition was not clear because sufficiently high N<sub>2</sub>O decomposition was observed without char feed.



# Anticipated problem with char transportation

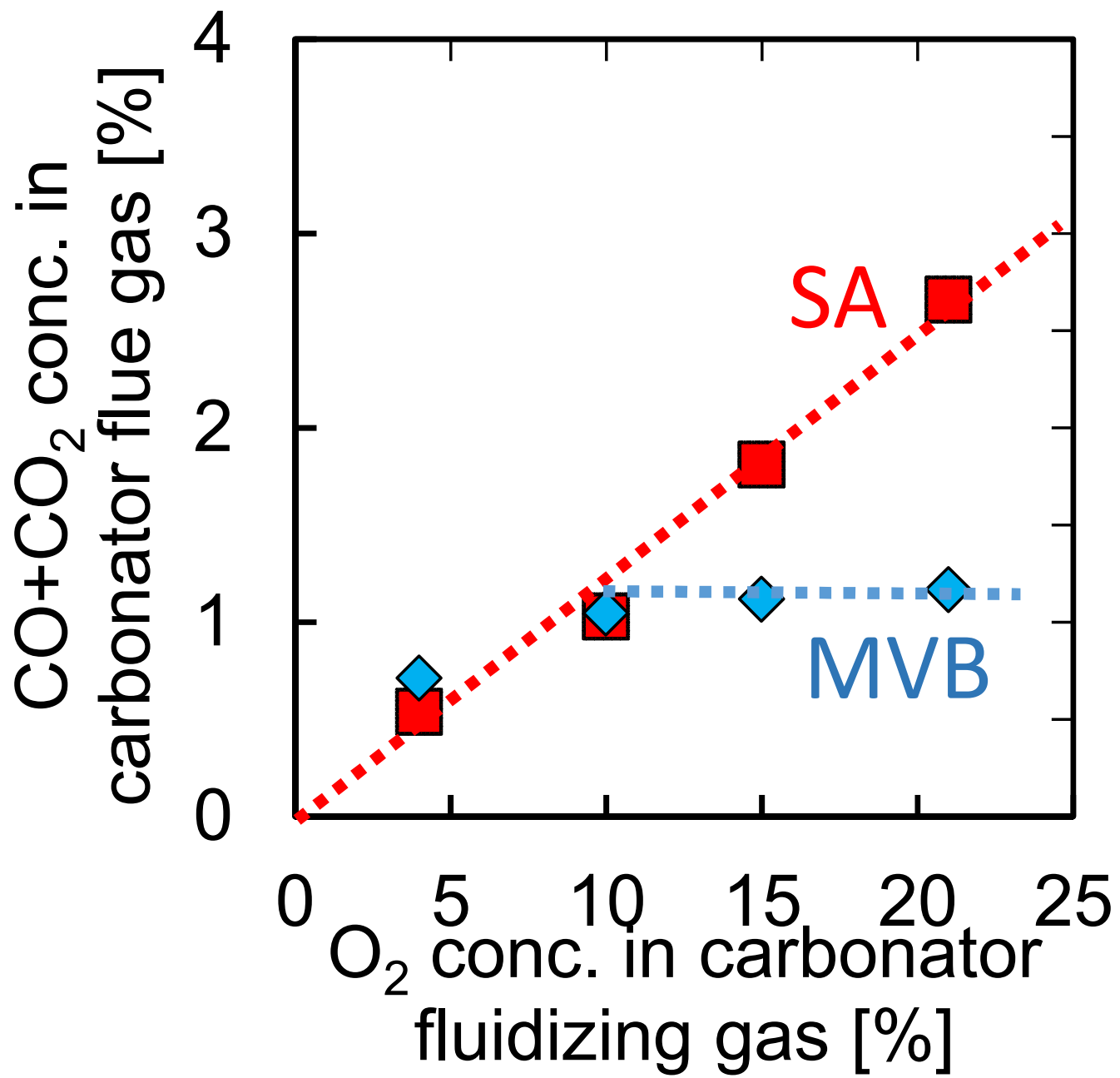
Transportation of char to carbonator

→ Low temperature oxidation of char → Formation of CO



# Formation of CO and CO<sub>2</sub> in carbonator (dual-FB)

Char transportation to carbonator → CO & CO<sub>2</sub> formation when sand was employed as bed material for dual-FB experiments.

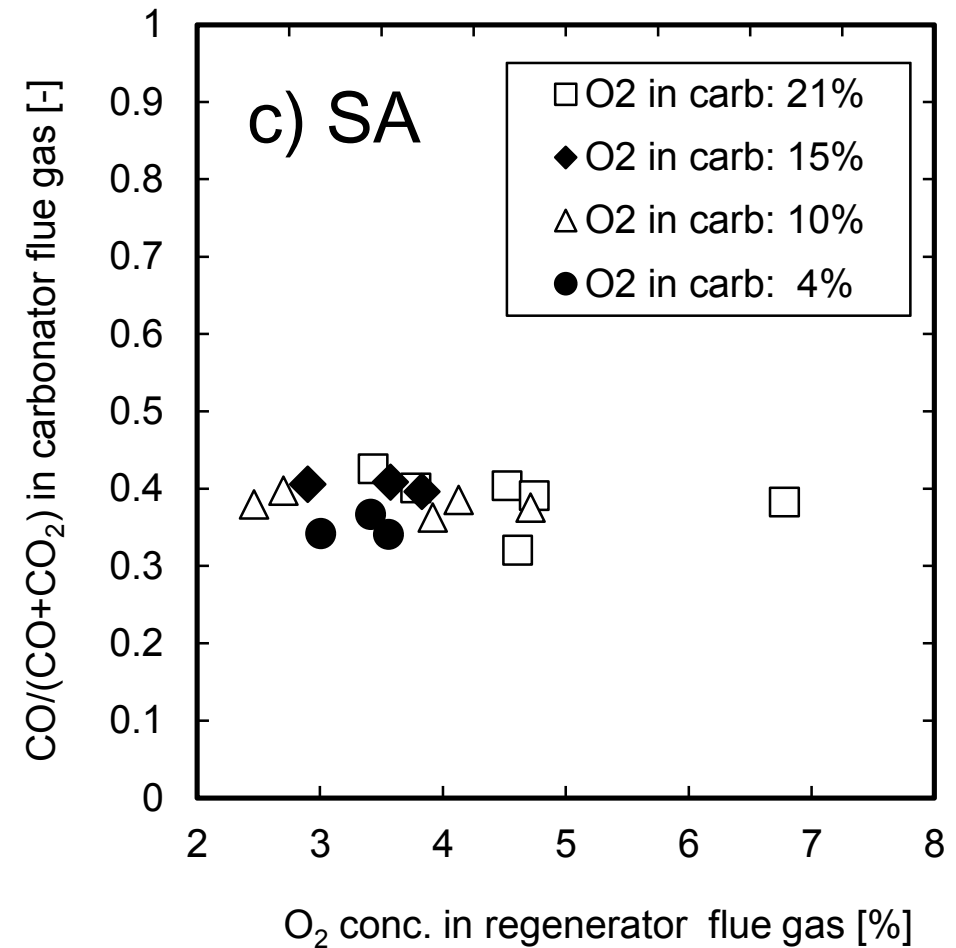
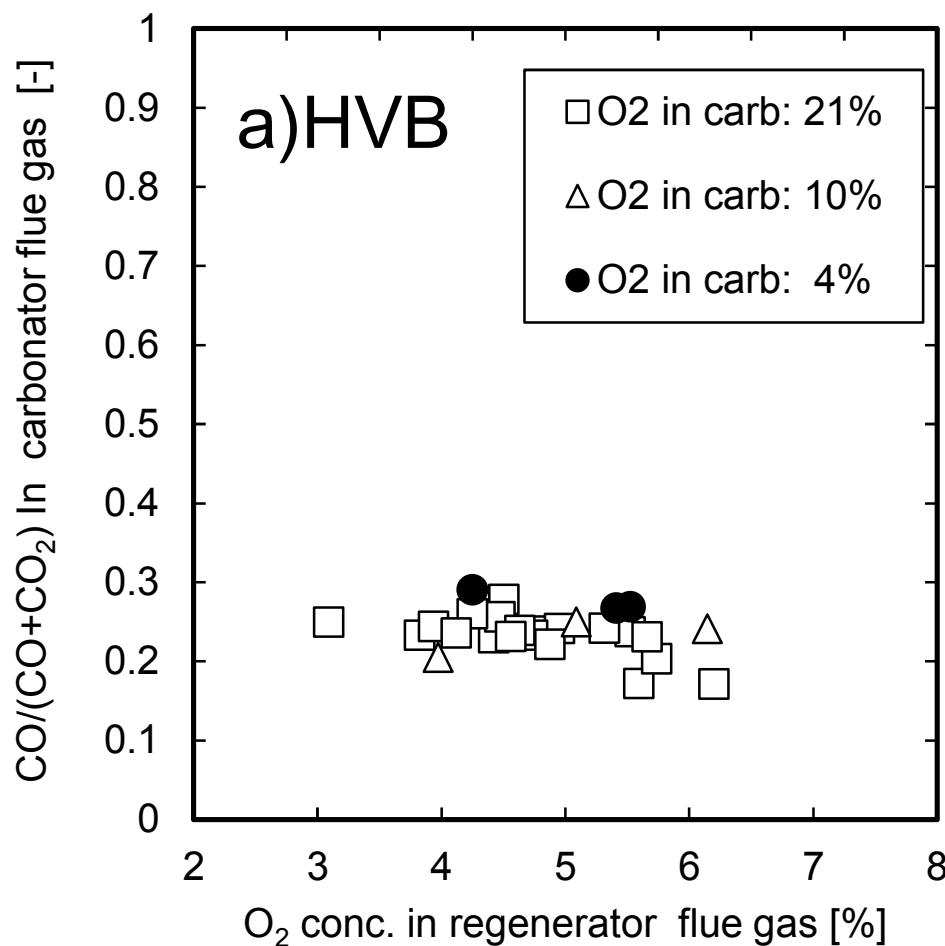


(Shimizu et al., J. Jpn. Inst. Energy, 94, 841-850, 2015)

# Previous results of CO emissions from carbonator

When sand was employed as bed material, 20 – 40% of carbon oxidized in the carbonator was converted to CO.

→ CO in gas = 1000 – 2000 ppm



(Shimizu et al., J. Jpn. Inst. Energy, 94, 841-850, 2015)

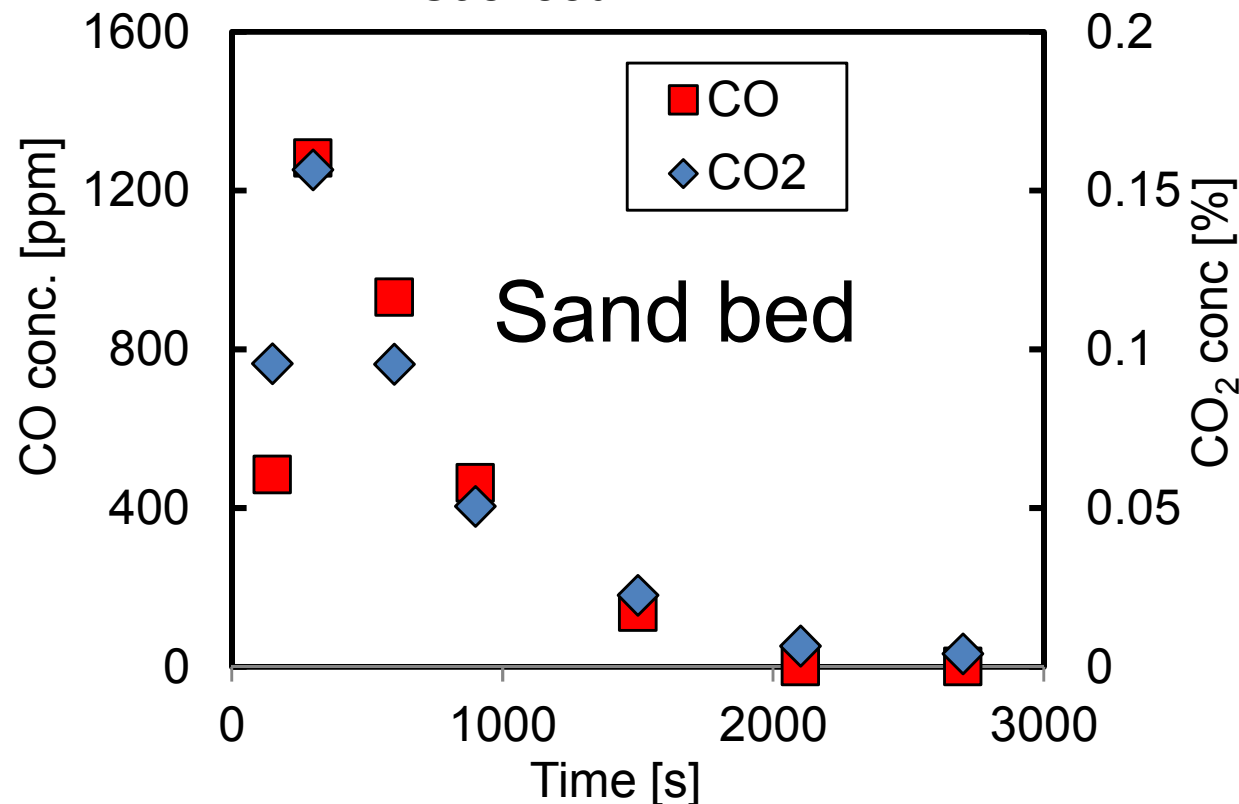
# Present results of CO formation from char

Selectivity to CO was reduced from 0.45 for sand bed (similar to dual-FB results) to zero (<detection limit) for CaO bed. CaO bed can suppress CO emissions even when char is transported to carbonator.

## Selectivity to CO

Sand bed	CaO bed
0.45	0

Sand bed, O<sub>2</sub> 8%, Char 42.2 mg,  
Gas feed 1.7 NL/min



# Conclusions

It is expected that carbonator of CaL process can work as  $\text{N}_2\text{O}$  abatement reactor because CaO can work as  $\text{N}_2\text{O}$  decomposition catalyst.

Char particles are known to be transported from regenerator to carbonator and form CO there.

The presence of CaO is expected to reduce CO emissions from carbonator.

# Acknowledgements

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